

## Recent progress with superconducting undulators at ANKA

Sara Casalbuoni

for

S. Casalbuoni<sup>1</sup>, T. Baumbach<sup>1</sup>, S. Gerstl<sup>1</sup>, A. Grau<sup>1</sup>, M. Hagelstein<sup>1</sup>,  
C. Heske<sup>1</sup>, T. Holubek<sup>1</sup>, D. Saez de Jauregui<sup>1</sup>, C. Boffo<sup>2</sup>, W. Walter<sup>2</sup>

<sup>1</sup>Karlsruhe Institute of Technology, Karlsruhe, Germany

<sup>2</sup>Babcock Noell GmbH, Würzburg, Germany

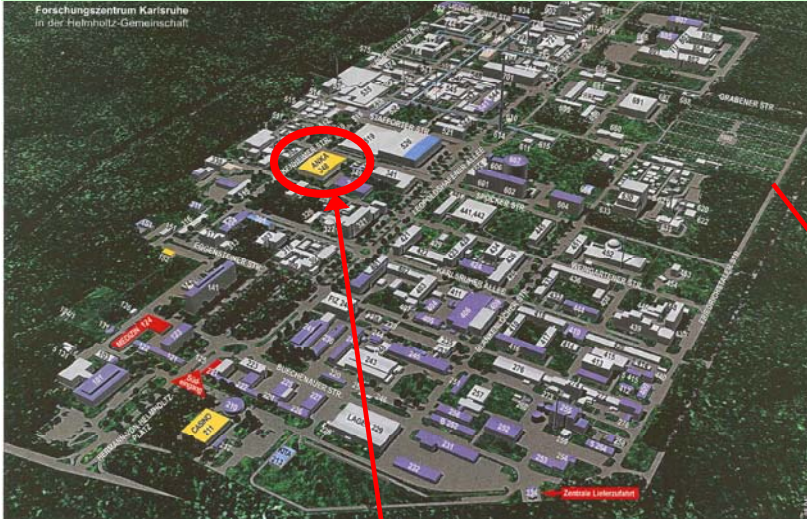
ISS/ANKA



- **Introduction**
  - ANKA
  - Motivation R&D of SCIDs
  
- **Superconducting undulator**
  
- **Period length switching**
  - Experimental demonstration of feasibility
  - Superconducting switch
  
- **New materials**
  
- **Tools and instruments for R&D**
  - CASPERI
  - CASPERII
  - COLDDIAG



## Karlsruhe Institute of Technology Campus North



**Energy:** 2.5 GeV  
**Current:** 200 mA  
**Circumference:** 110.4 m

### SCU14

- Proof of principle of scu technology first time worldwide demonstrated at ANKA (2005) developed in collaboration with ACCEL.
- Performance limited by too high beam heat load



# Motivation R&D of scIDs

Aim is to develop, manufacture, and test superconducting undulators to generate:

Harder X-ray spectrum

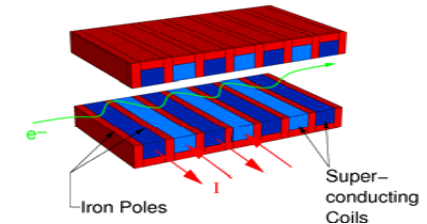
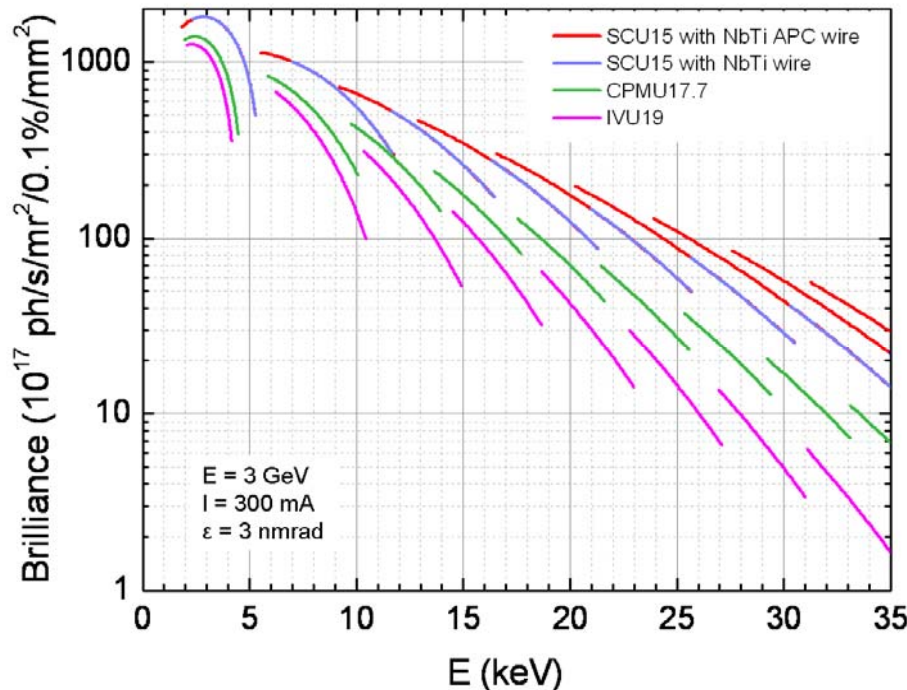
Higher brilliance X-ray beams

with respect to permanent magnet undulators.

Why?

Larger magnetic field strength for the same gap and period length.

Same magnetic length=2 m and vacuum gap=5mm



|                  | IVU* | CPMU† | SCU NbTi wire** | SCU NbTi APC†† |
|------------------|------|-------|-----------------|----------------|
| $\lambda_u$ [mm] | 19   | 17.7  | 15              | 15             |
| N                | 105  | 112   | 133             | 133            |
| m. gap [mm]      | 5    | 5.2   | 6               | 6              |
| B [T]            | 0.86 | 1.04  | 1.2             | 1.46           |
| K                | 1.53 | 1.72  | 1.7             | 2.05           |

\*F. Bødker et al., EPAC06

†C.W. Osterfeld & M. Pedersen, IPAC10

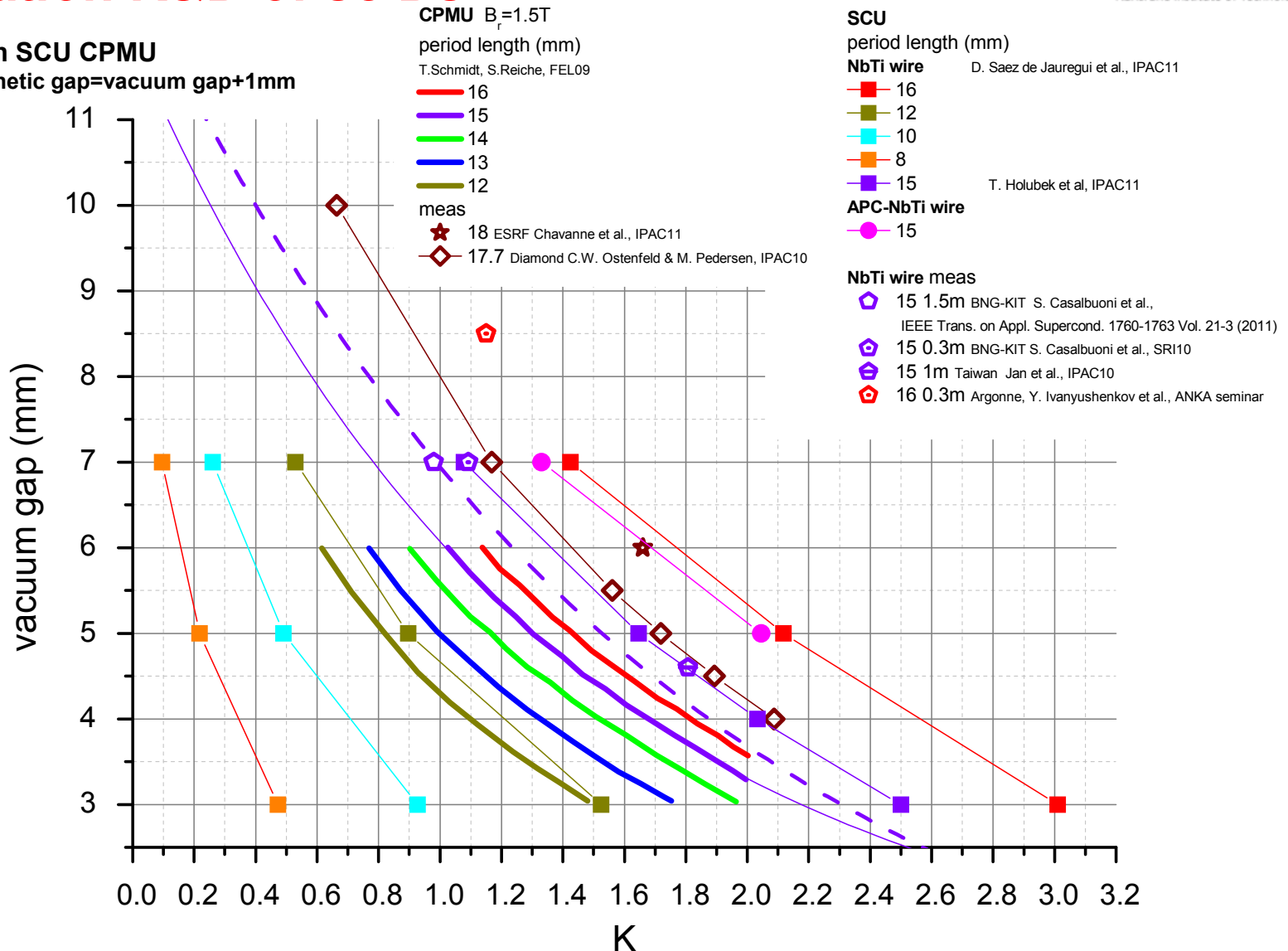
\*\*D. Saez de Jauregui et al., IPAC11

††T. Holubek et al., IPAC11

A given photon energy can be reached by the SCU with lower order harmonic:  
 20 keV reached with the 7<sup>th</sup> harm. of SCU, with the 9<sup>th</sup> harm. of CPMU and of IVU

# Motivation R&D of scIDs

Comparison SCU CPMU  
for SCU magnetic gap=vacuum gap+1mm



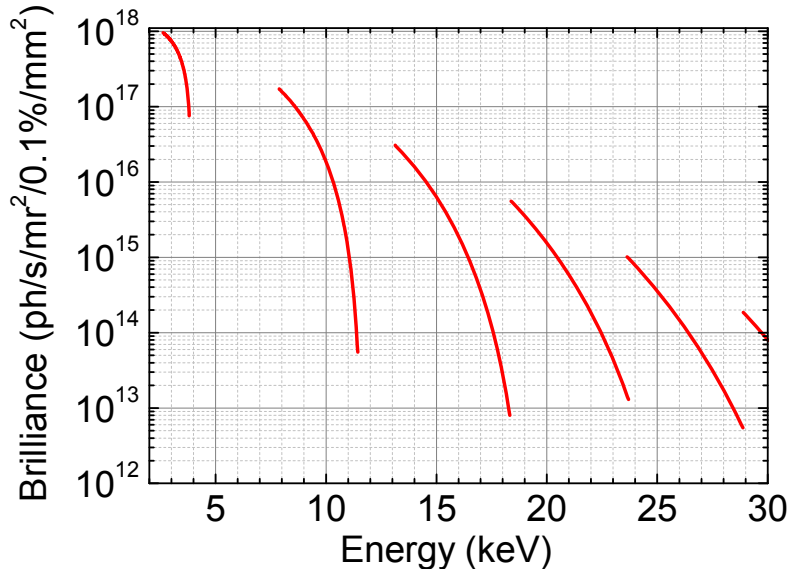


# New superconducting undulator demonstrator to be tested at ANKA

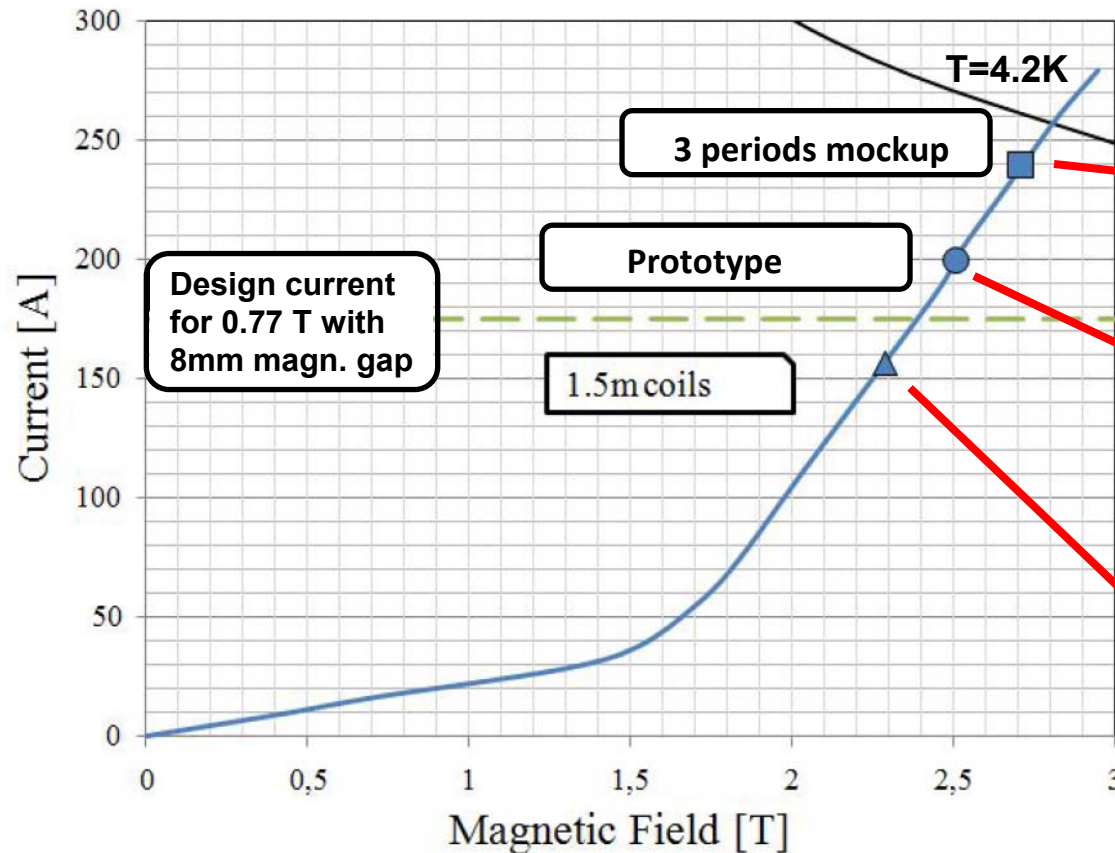
Under development in collaboration with BNG

|  |        |
|--|--------|
| Period length                            | 15 mm  |
| Number of full periods                   | 100.5  |
| Max field on axis with 8 mm magnetic gap | 0.69 T |
| Max field in the coils                   | 2.4 T  |
| Operating magnetic gap                   | 8 mm   |
| Operating beam gap                       | 7 mm   |
| Gap at beam injection                    | 16 mm  |
| Design beam heat load                    | 4W     |

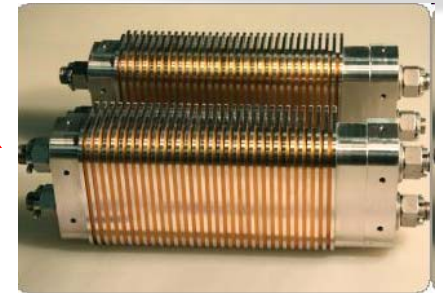
- Cryogen free magnet
- NbTi superconductor
- Integral field compensation
- Passive quench protection



# SCU15 demonstrator: magnet loadline



Measured @KIT

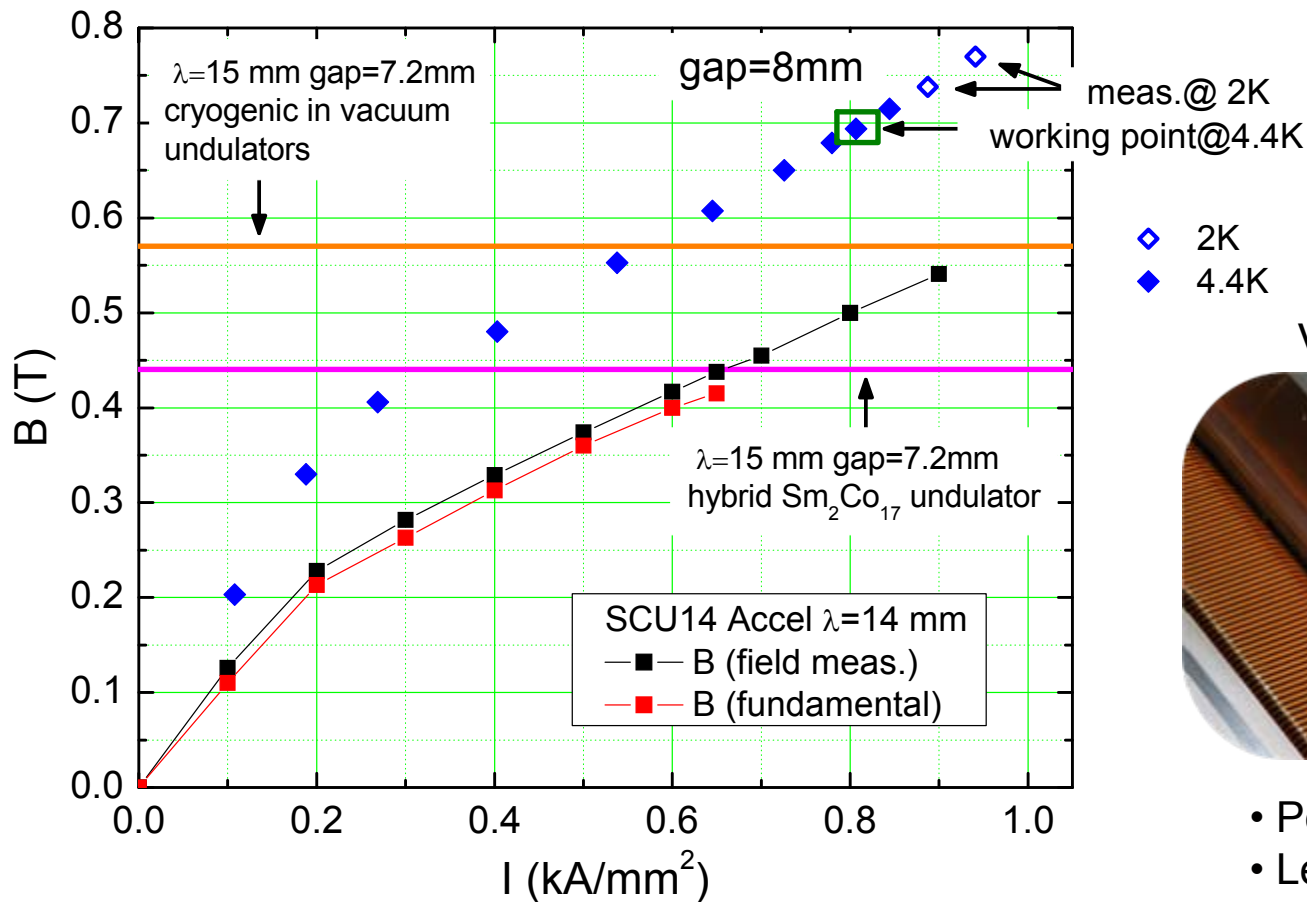


Measured @CERN

C. Boffo et al., IEEE Trans. on Appl. Supercond. 1756-1759 Vol. 21-3 (2011)

# SCU15 demonstrator

## Comparison with competing technologies and with SCU14 demonstrator



◇ 2K  
◆ 4.4K

vacuum gap=7 mm



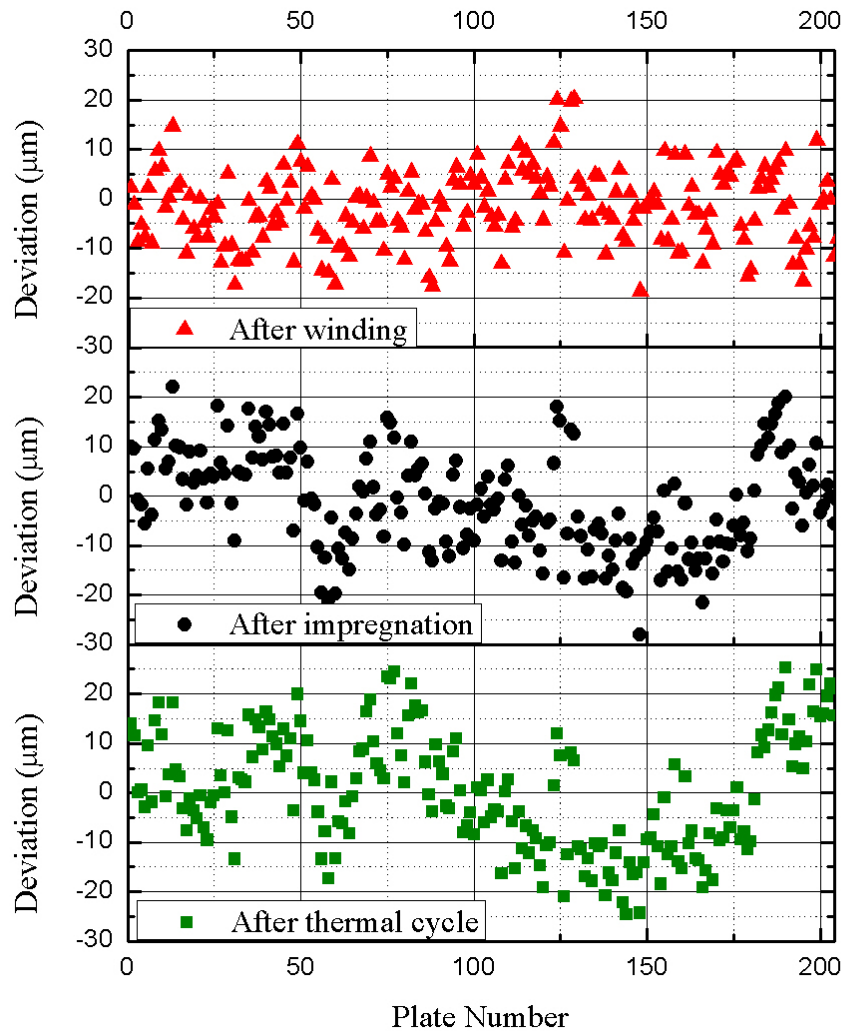
- Period length: 15 mm
- Length: 100 periods
- NbTi - coils

S.C. et al., IEEE Trans. on Appl. Supercond. 1760-1763 Vol. 21-3 (2011)



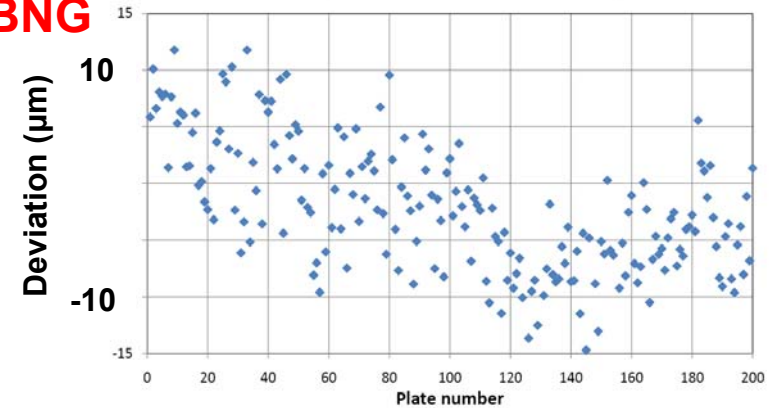
# Accuracies measured @300K

## Yoke 2 Planarity

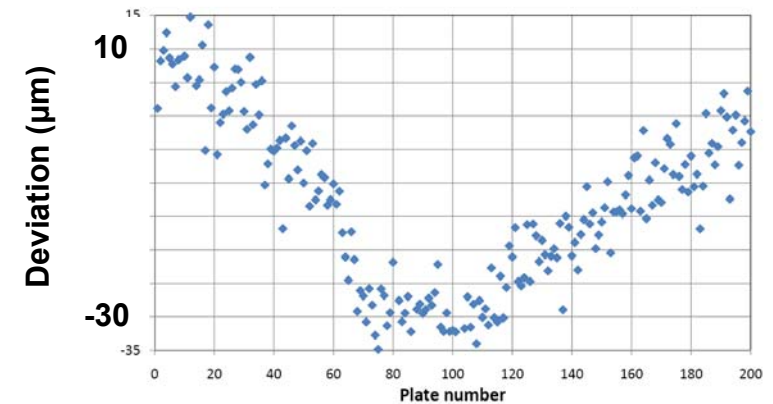


by BNG

Period length deviation within a magnet



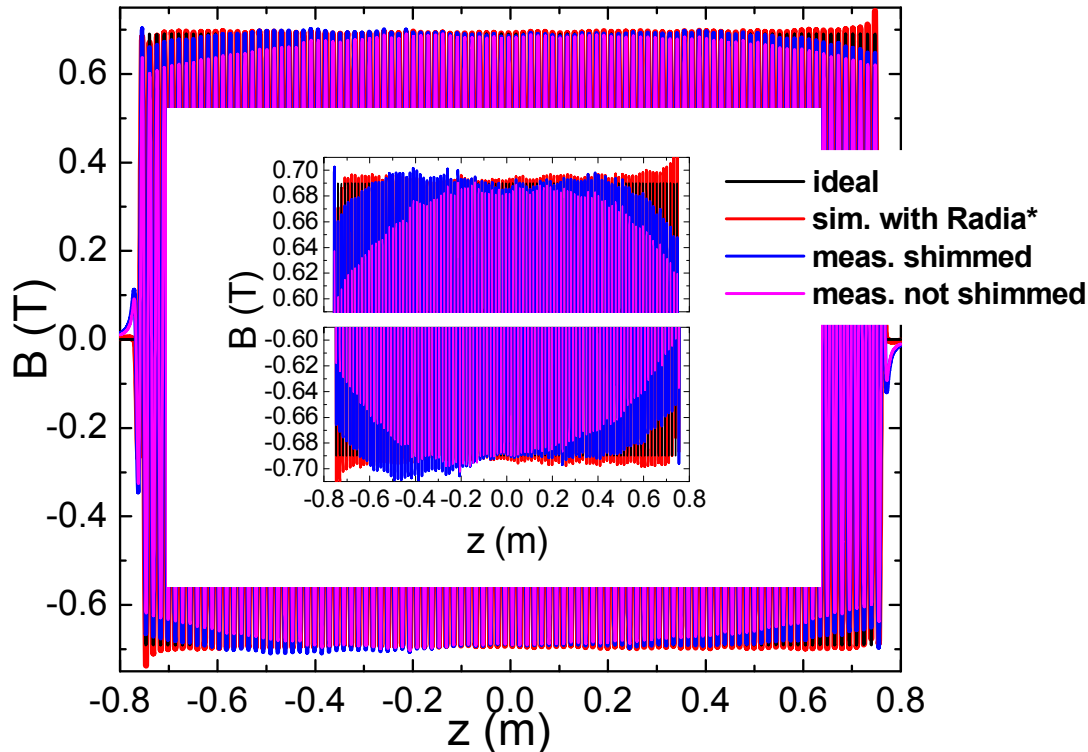
Period length shift within magnets



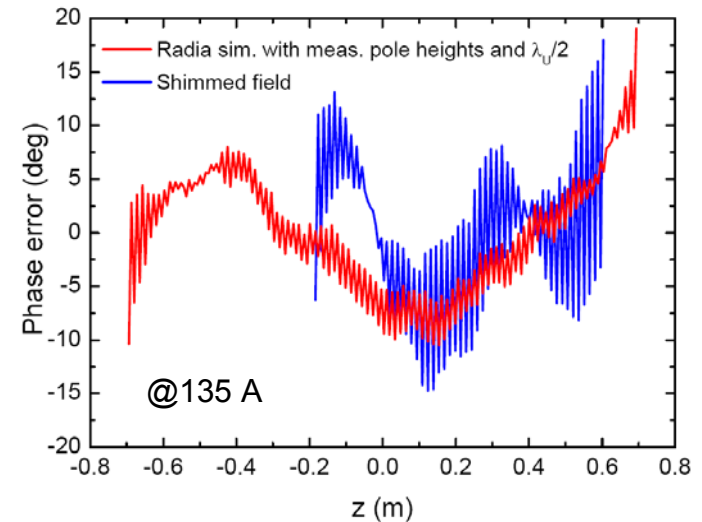
- WINDING POSITIONING ACCURACY:** 40 μm
- POLE LONGITUDINAL POSITION:** 30 μm
- LENGTH DIFFERENCE BETWEEN COILS:** 20 μm
- COIL PLANARITY ALONG 1.5 M :** 50 μm
- GAP DIMENSION AT ENDS DEVIATION:** 10 μm

C. Boffo et al., IEEE Trans. on Appl. Supercond. 1756-1759 Vol. 21-3 (2011)

# SCU15 demonstrator: phase error



Stainless steel support structure, which fixes the magnetic gap at room temperature to  $8 \pm 0.01$  mm.



## Shimmed field:

Phase error of 7.4 degrees over a length of  $\sim 0.8$  m

**Radia\* simulations with meas. pole heights and half period lengths at 300K ( $\sim 50\mu\text{m}$ ):**

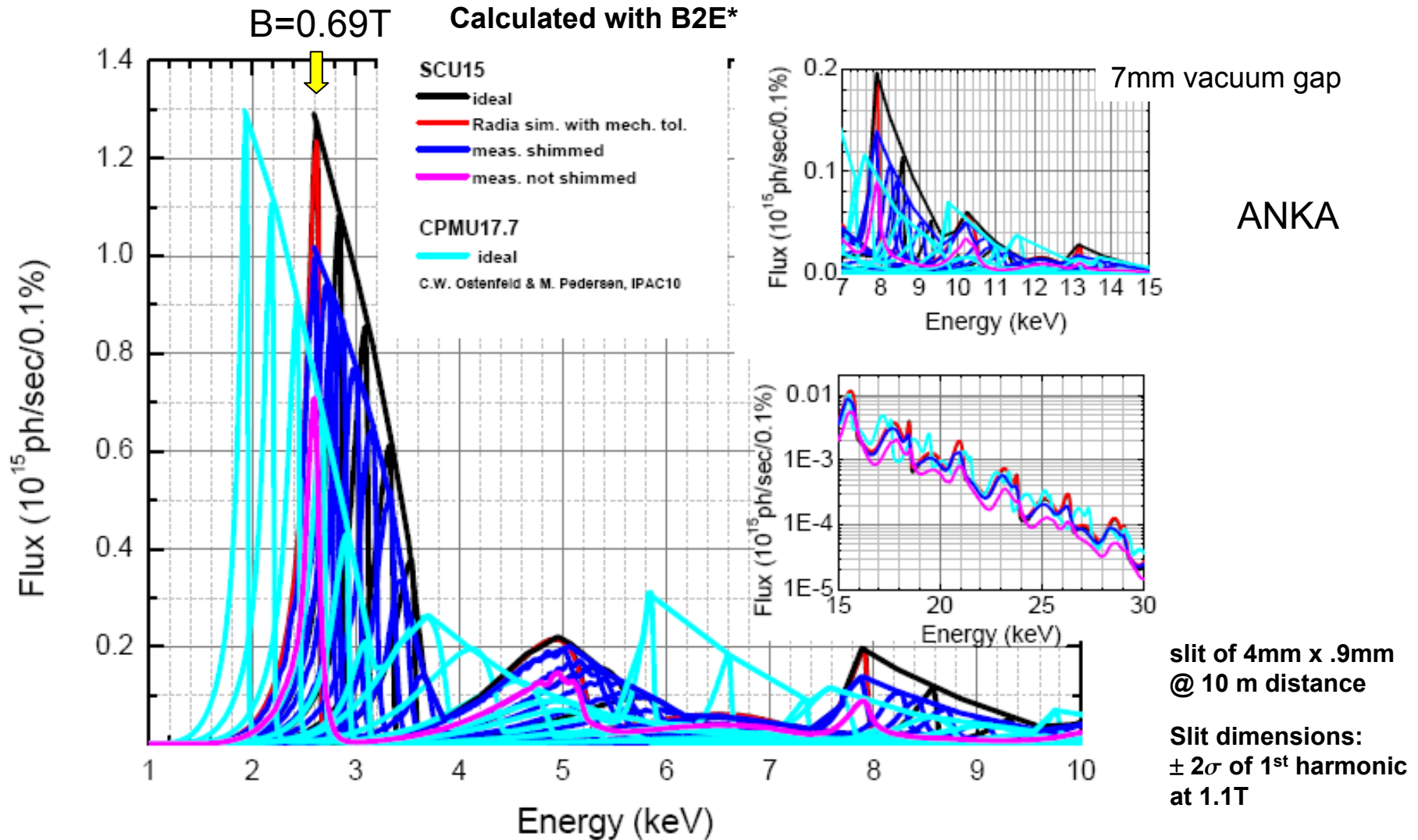
Phase error of 5.6 degrees over a length of  $\sim 1.4$  m

The use of mechanical shims to reduce the bimetallic effect, applicable to fixed gap undulators, together with a planarity further reduced to  $40 \mu\text{m}$  would make it possible to reach 3.5 degrees phase error without additional correction coils.

\*P. Elleaume, O. Chubar, J. Chavanne, PAC97

S.C. et al., IEEE Trans. on Appl. Supercond. 1760-1763 Vol. 21-3 (2011)

# SCU15 demonstrator: spectral performance

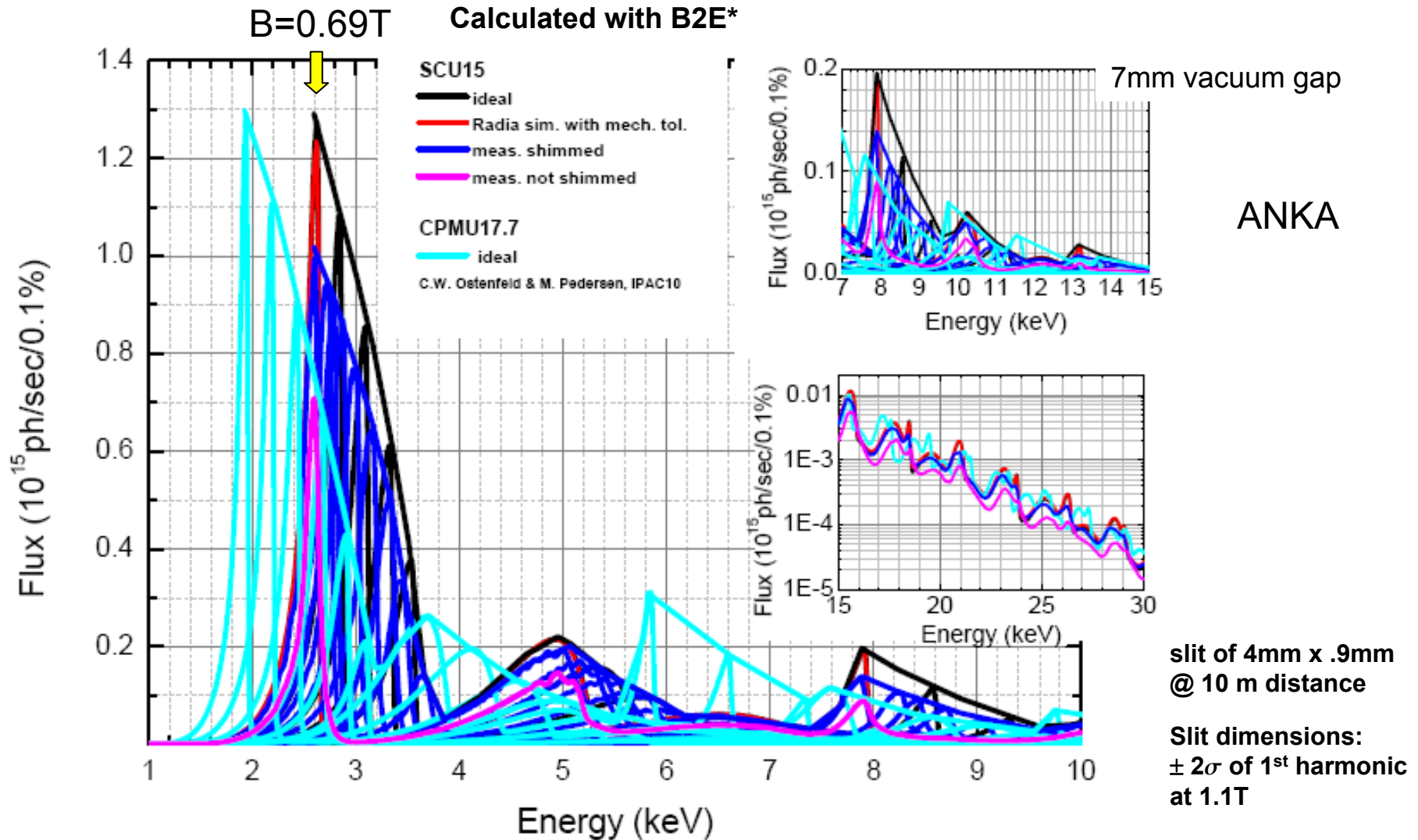


\*P. Elleaume, X. Marechal, Report ESRF-R/ID-9154 (1991)

S.C. et al., to appear in IPAC12



# SCU15 demonstrator: spectral performance

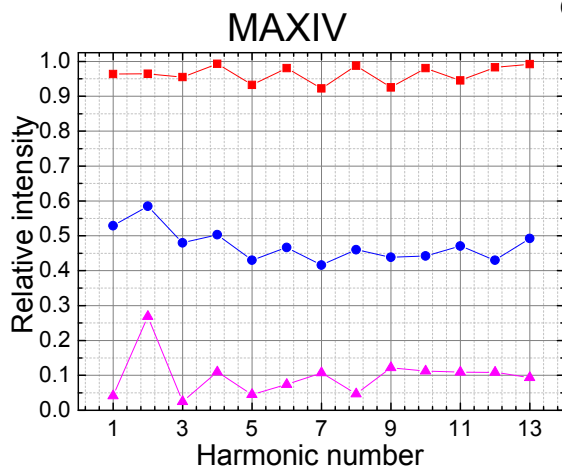
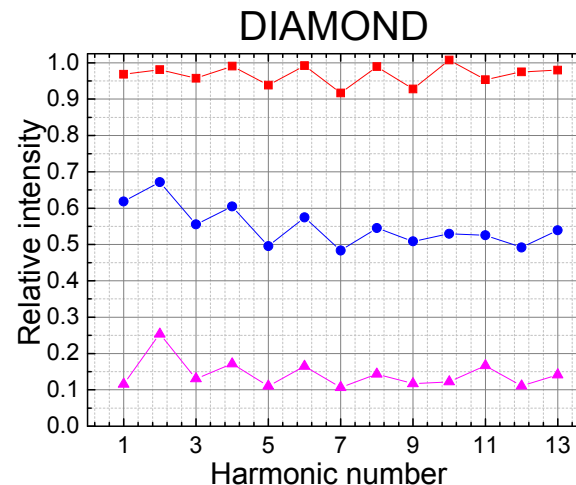
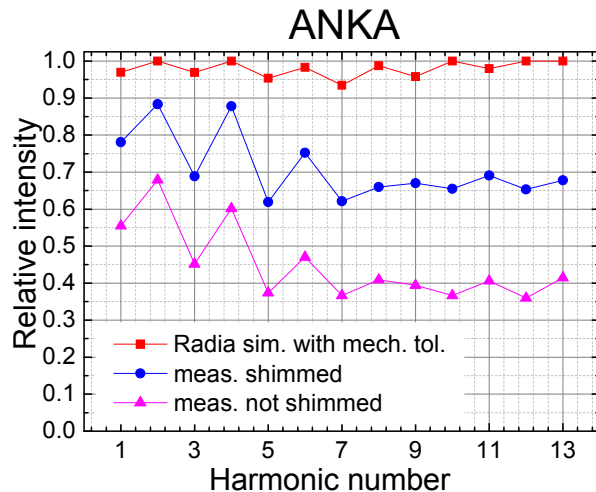


\*P. Elleaume, X. Marechal, Report ESRF-R/ID-9154 (1991)

S.C. et al., to appear in IPAC12

# SCU15 demonstrator: spectral performance

Ratio of flux of different harmonics to spectrum calculated used ideal field



SCU  $\lambda_u=15\text{mm}$   $N_{\text{periods}}=101$   
 CPMU  $\lambda_u=17.7\text{ mm}$   $N_{\text{periods}}=87$

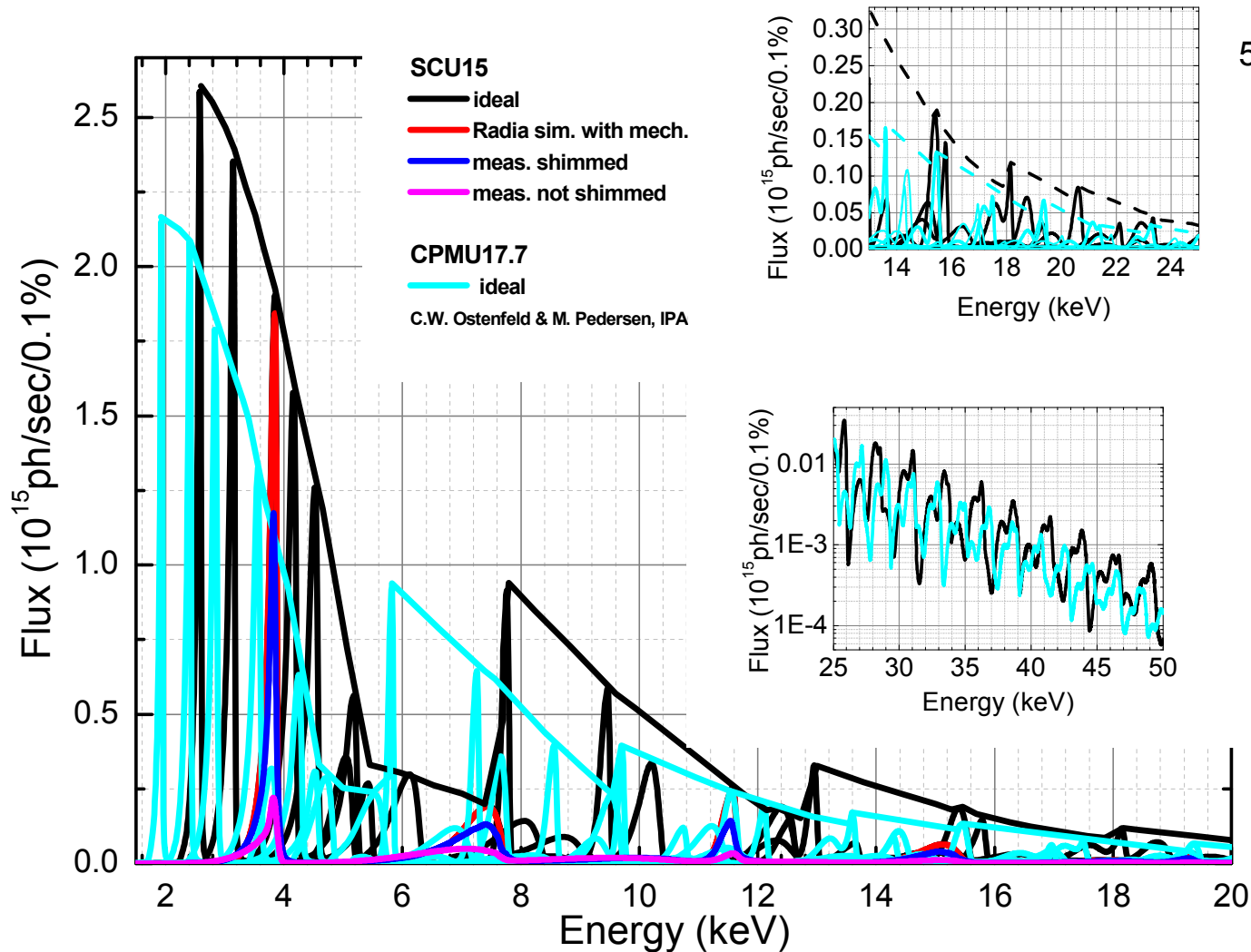
|                                     | ANKA* | DIAMOND † | MAXIV** |
|-------------------------------------|-------|-----------|---------|
| E (Gev)                             | 2.5   | 3         | 3       |
| I (A)                               | 0.2   | 0.3       | 0.5     |
| $\Delta E/E$                        | 0.001 | 0.001     | 0.001   |
| $\epsilon_x$ (nm rad)               | 41    | 2.7       | 0.26    |
| $\epsilon_y$ (nm rad)               | 0.3   | 0.27      | 0.008   |
| $\beta_x$ (m)                       | 14.7  | 4.8       | 9       |
| $\beta_y$ (m)                       | 1.93  | 1.43      | 4.8     |
| $\eta_x$ (m)                        | 0.36  | 0.07      | 0       |
| vac. Gap                            | 7     | 5         | 4       |
| $B_{\text{max}}_{\text{SCUideal}}$  | 0.69  | 1.1       | 1.4     |
| $B_{\text{max}}_{\text{CPMUideal}}$ | 0.707 | 1.04      | 1.263   |

\* A. S. Müller, priv. comm.  
 † I. P. S. Martin et al, PAC07  
 \*\* S. C. Leemann et al.,  
 Phys. Rev. ST Accel.  
 Beams, 12:120701, 2009

S.C. et al., to appear in IPAC12

# SCU15 demonstrator: spectral performance

Calculated with B2E\*



5mm vacuum gap

DIAMOND

slit of 1.2mm x .6mm  
@ 10 m distance

Slit dimensions:  
 $\pm 2\sigma$  of 1<sup>st</sup> harmonic  
at 1.1T

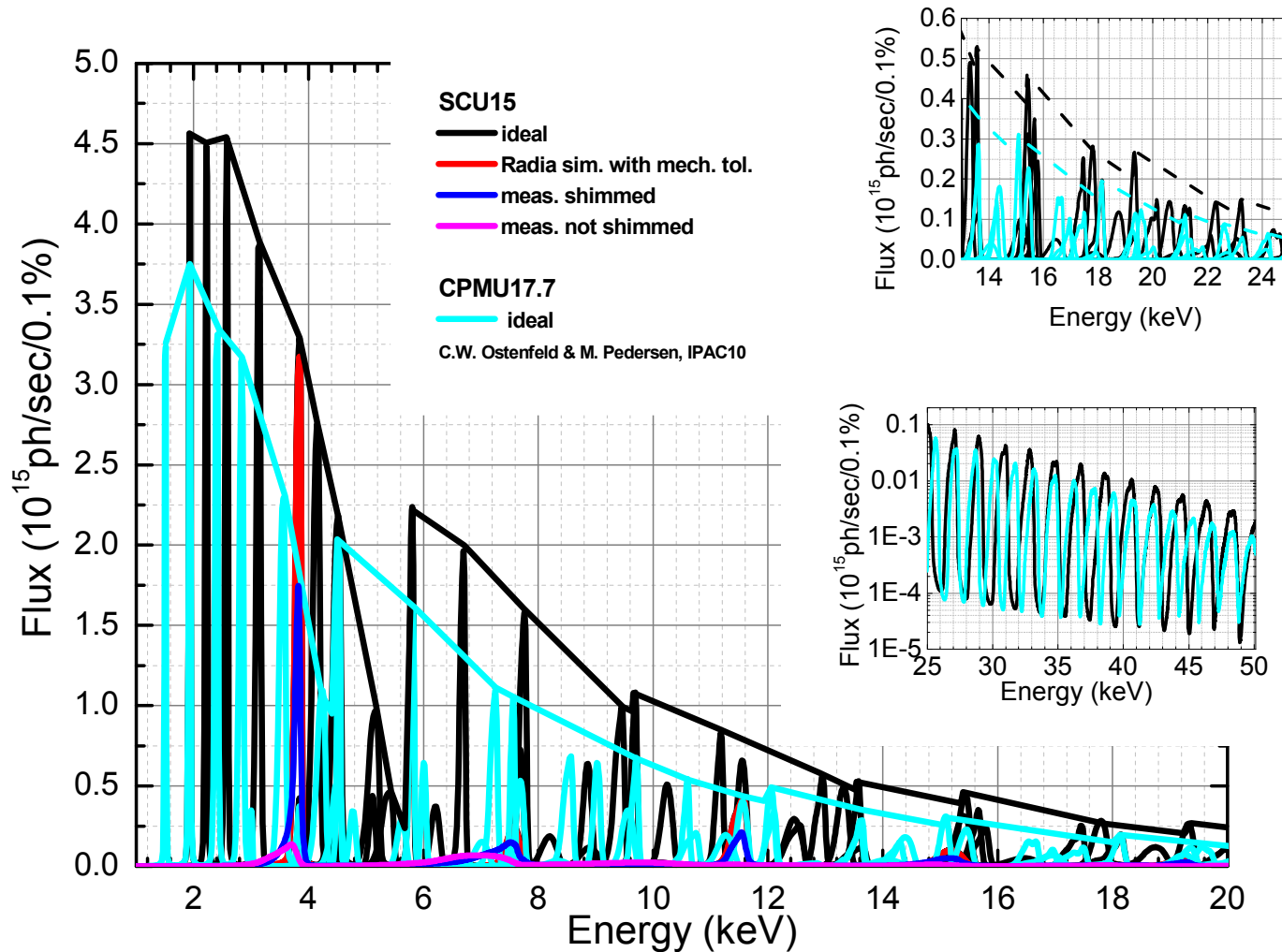
\*P. Elleaume, X. Marechal, Report ESRF-R/ID-9154 (1991)

S.C. et al., to appear in IPAC12



# SCU15 demonstrator: spectral performance

Calculated with B2E\*



4mm vacuum gap

MAXIV

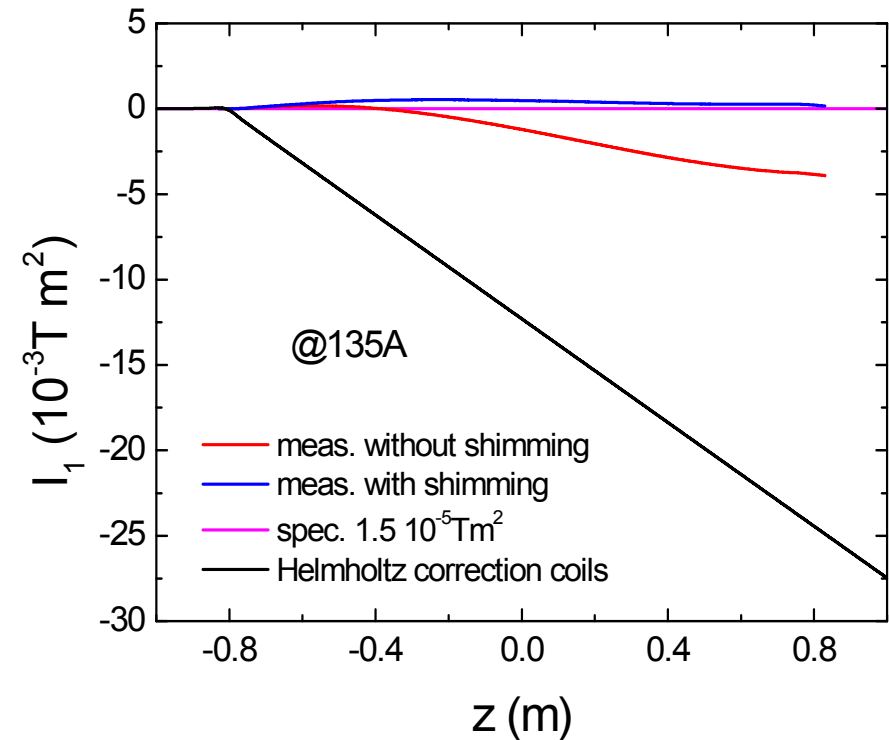
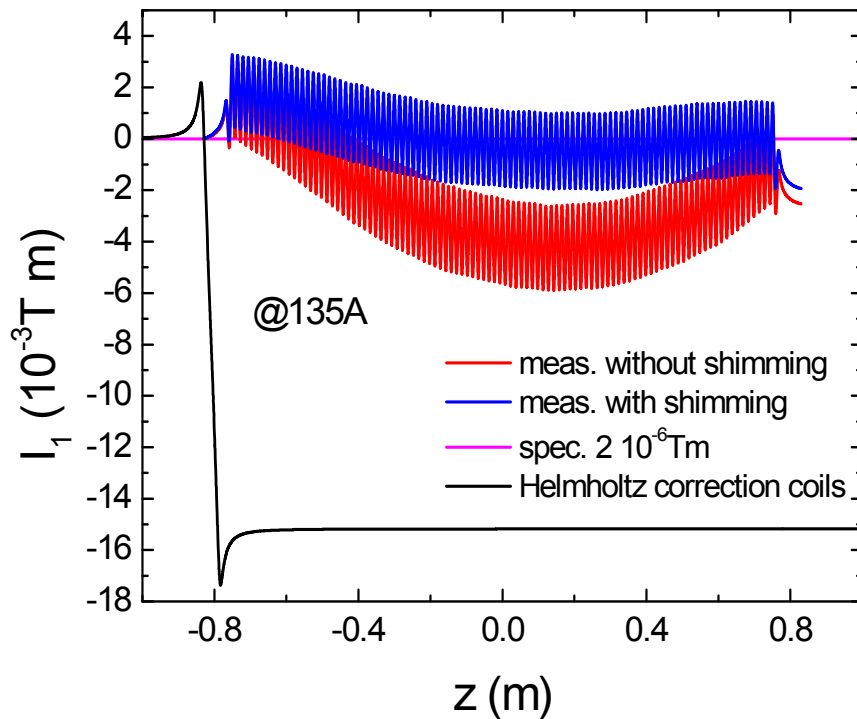
slit of .68 mm x .64 mm  
@ 10 m distance

Slit dimensions:  
 $\pm 2\sigma$  of 1<sup>st</sup> harmonic  
at 1.4T

\*P. Elleaume, X. Marechal, Report ESRF-R/ID-9154 (1991)

S.C. et al., to appear in IPAC12

# SCU15 demonstrator: field integrals



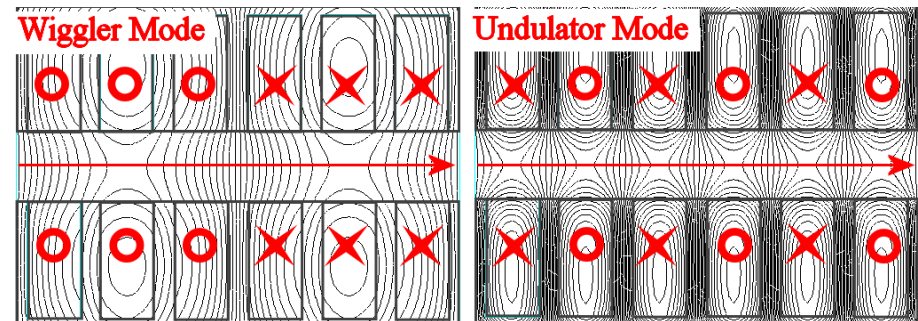
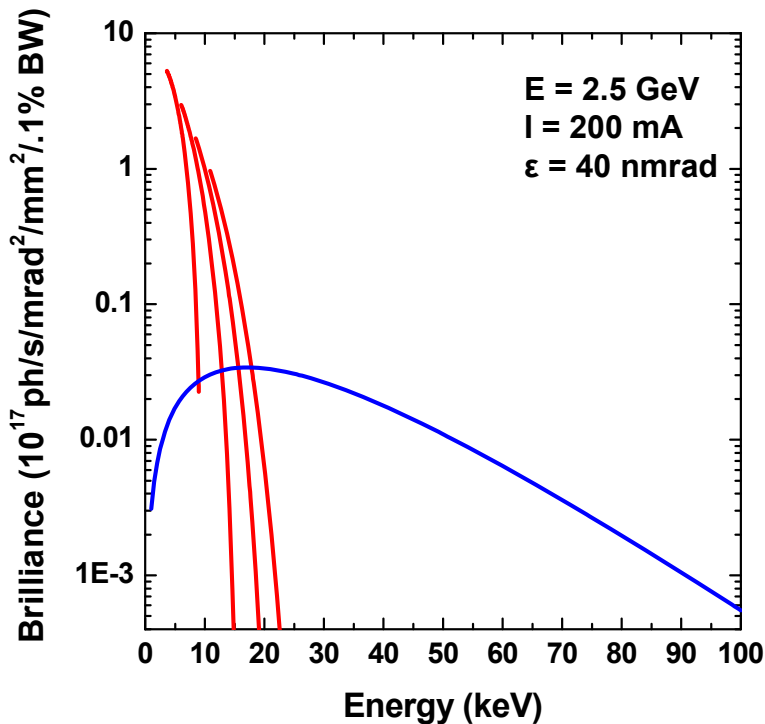
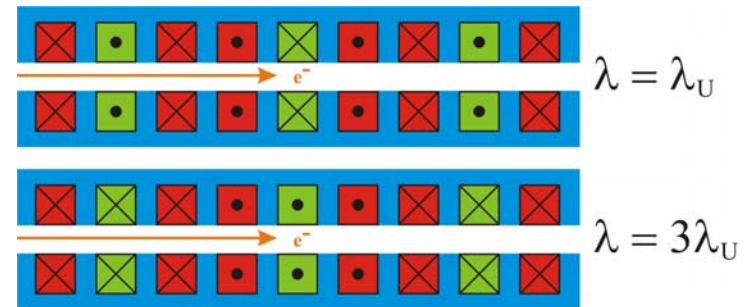
For all currents it is possible to correct the first and second field integrals by means of two pair of Helmholtz coils.

S.C. et al., IEEE Trans. on Appl. Supercond. 1760-1763 Vol. 21-3 (2011)

# Sc Undulator Wiggler

A device which allows switching between a 18 mm period length undulator and a 54 mm wiggler.

- R. Schlueter et al., Synch. Rad. News, 2004
- B. Kostka et al., PAC05, 2005
- A. Bernhard et al., EPAC06, 2006
- A. Bernhard et al., EPAC08, 2008
- T. Holubek et al., IPAC11, 2011



Foreseen for the planned IMAGE beamline at ANKA.

## Applications:

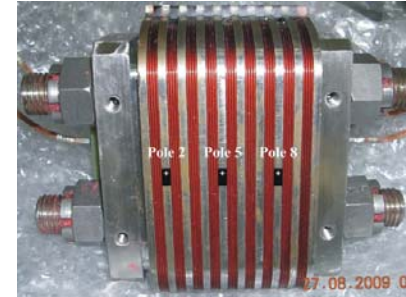
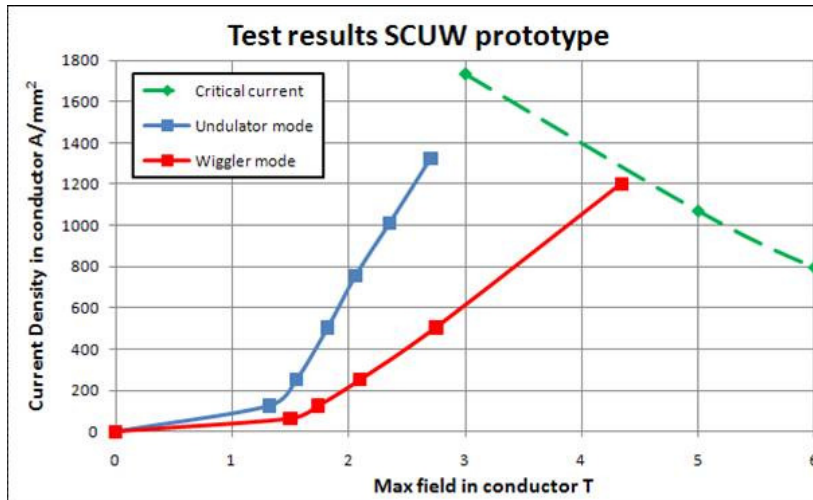
- High brilliance of the **undulator** from 6 to 15 keV for imaging,
- **wiggler** mode for higher photon energies to perform phase contrast tomography.



# Sc Undulator Wiggler

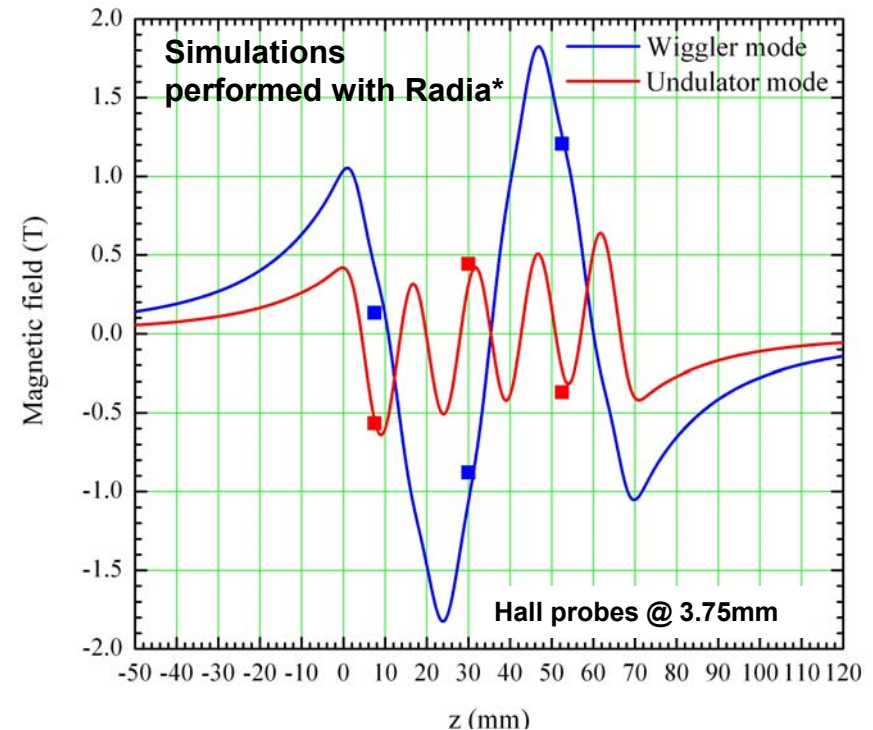
First experimental demonstration of period length switching for scIDs

## Training



Built by BNG

|          | undulator |      | wiggler |      |
|----------|-----------|------|---------|------|
|          | B (T)     | K    | B(T)    | K    |
| Mag. Gap |           |      |         |      |
| 8 mm     | 0.77      | 1.08 | 3.00    | 12.6 |
| 5 mm     | 1.46      | 2.05 | 4.34    | 18.2 |



A. Grau et al., IEEE Trans. on Appl. Supercond. 1596-1599 Vol. 21-3 (2011)

\*P. Elleaume, O. Chubar, J. Chavanne, PAC97

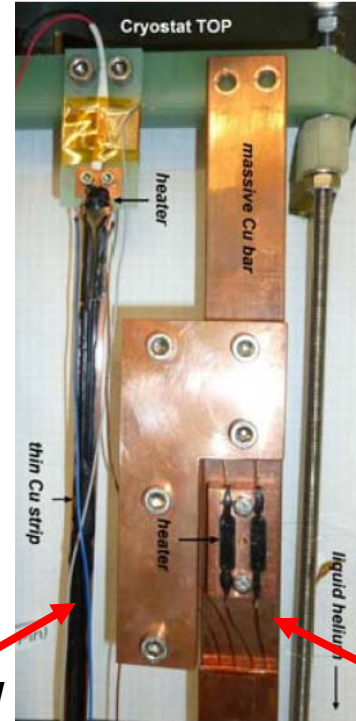
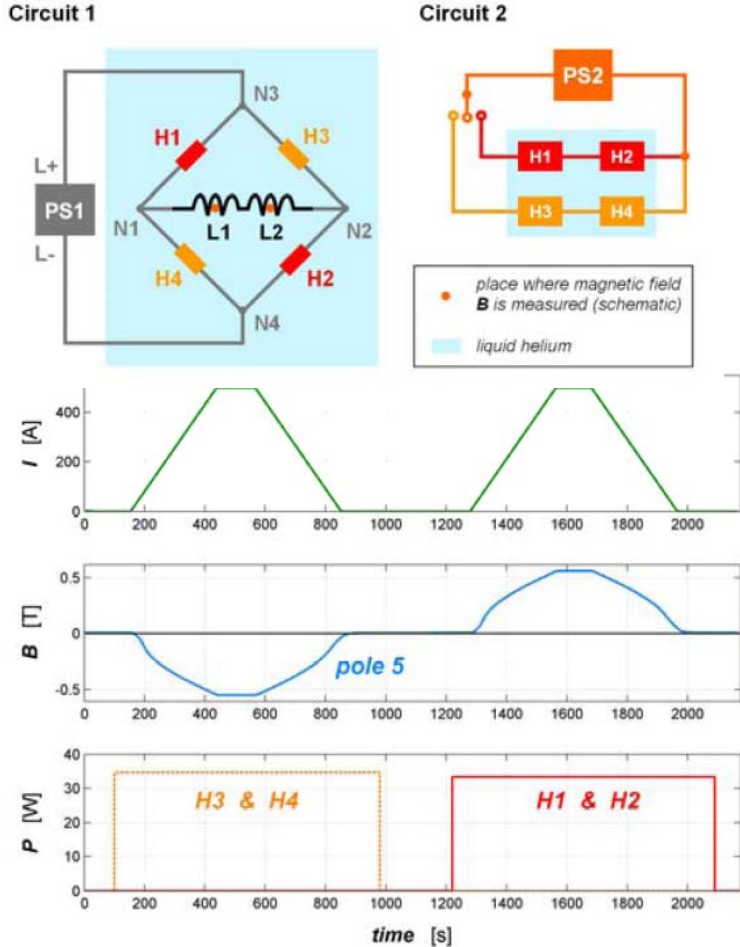
# Sc Undulator Wiggler: Superconducting switch

To use only one power supply instead of two for the two circuits, reducing the thermal input to the device

In liquid helium

Conduction cooled

Reproduced results of A. Madur et al., FEL2009

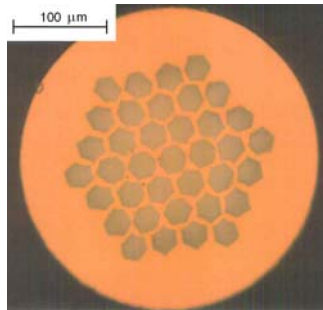


T. Holubek et al., IPAC11, 2011

Additional tests ongoing

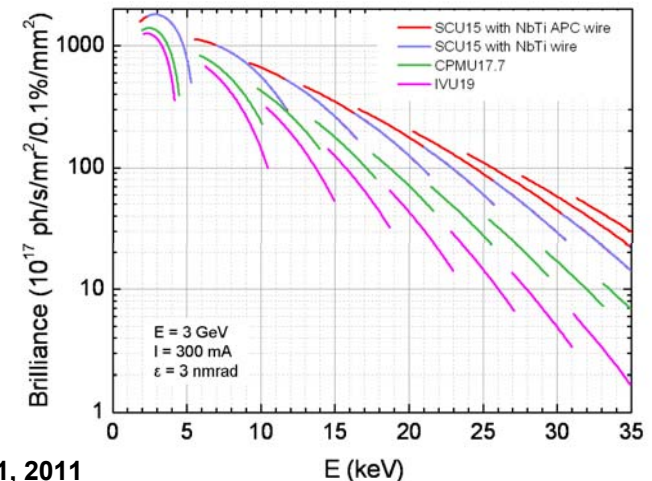
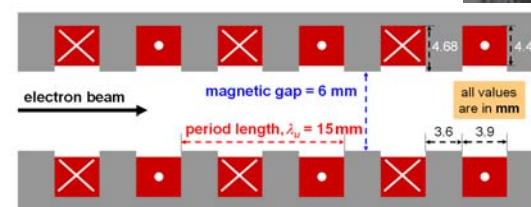
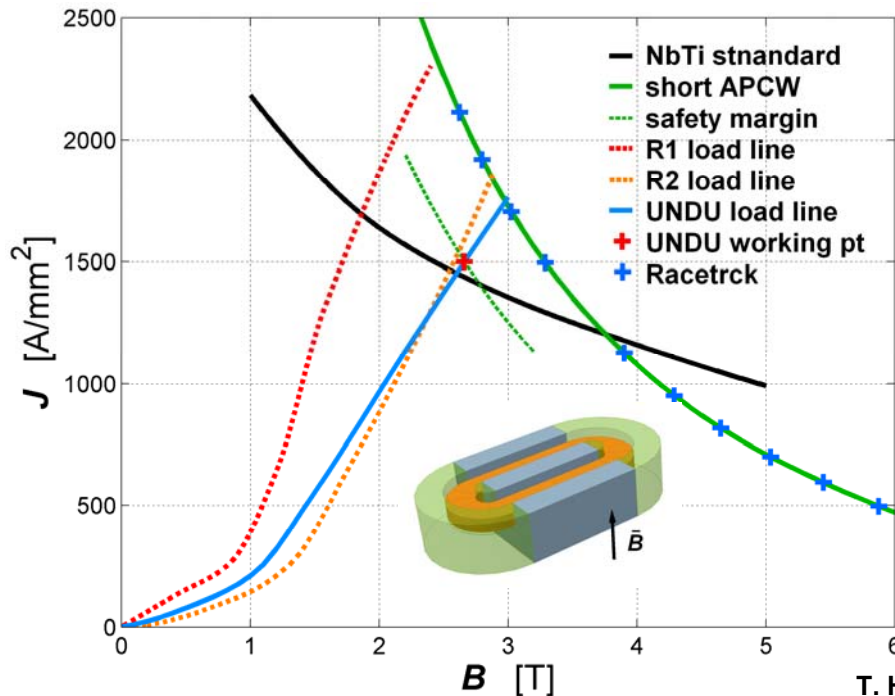
# New materials: NbTi with artificial pinning centers wire

ANKA collaboration with ITeP (Th. Schneider and M. Kläser, KIT ) and SupraMagnetics, Inc., USA



NbTi with artificial pinning centers wire developed by SupraMagnetics, Inc., USA:  
 outer diameter = 0.31 mm  
 Including insulation = 30 μm,  
 Cu/SC= 2.125  
 37 filaments with diameter = 21 μm

Racetrack loadline and wire critical current density measured at JUMBO (ITeP, KIT)

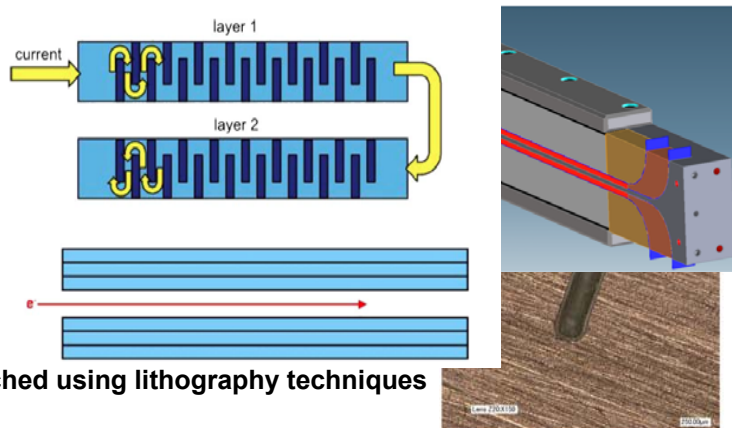


T. Holubek et al., IPAC11, 2011

# New materials: HTS tape

- The engineering current density of commercial HTS materials is rapidly increasing in performance making them more and more attractive, so that they could be competitive with NbTi.
- HTS tapes can be operated at higher temperatures than NbTi allowing to sustain higher beam heat loads, and therefore simplifying the cryostat design for the final device.
- High mechanical accuracy required for SC undulators in light sources exclude application of Nb<sub>3</sub>Sn coils with actual technology, that requires heat treatment after winding
- Two concepts of application of HTS tapes to produce a sinusoidal field have been so far proposed:

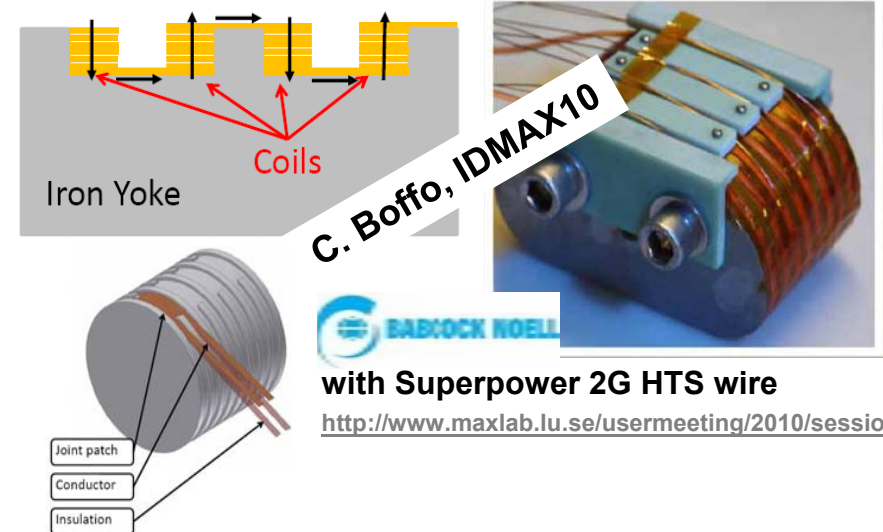
## HTS tape stacked undulator



Etched using lithography techniques

S. Prestemon et al., IEEE Trans. on Appl. Supercond. 1880-1883 Vol. 21-3 (2011)

## HTS tape planar undulator



with Superpower 2G HTS wire

<http://www.maxlab.lu.se/usermeeting/2010/sessions/>



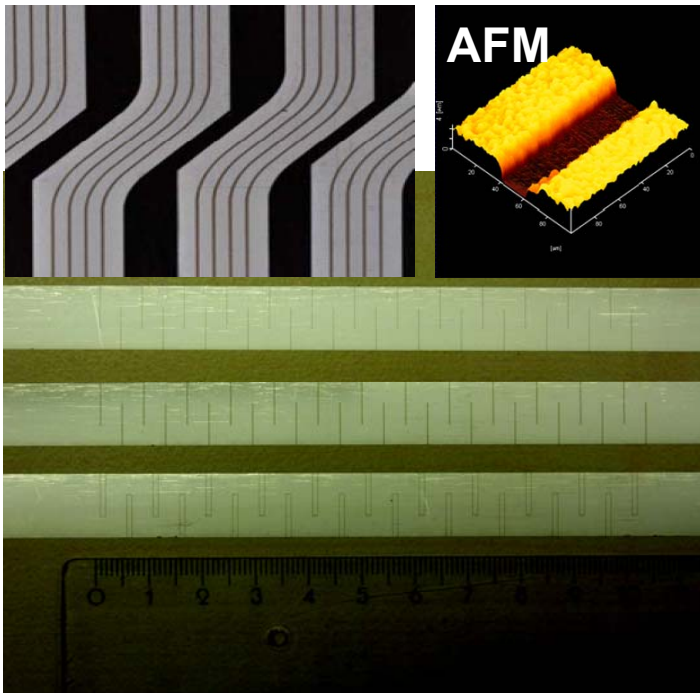
# New materials: HTS tape

## HTS tape stacked undulator

KIT internal collaboration:  
ANKA with ITeP (W. Goldacker)

Etching using Trumpf picosec YAG - IR laser,  
programmable beam control used for Roebel cables

Groove formation very reliable applying laser grooving  
No contamination of groove detected (SEM)

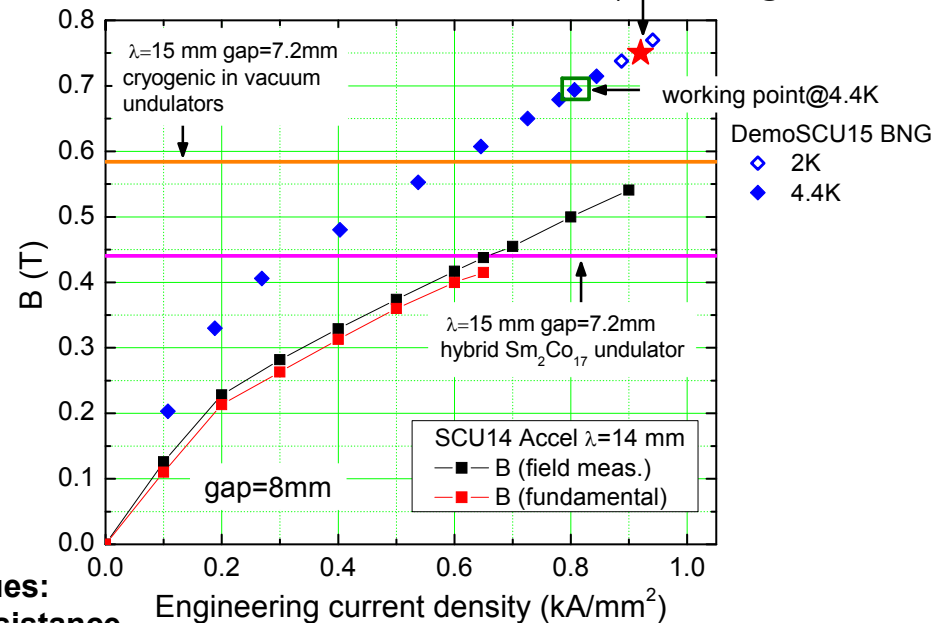


## HTS tape planar undulator

Babcock Noell GmbH (BNG)  
HTS tape planar undulator mockup:  
results of test at CASPERI (KIT)

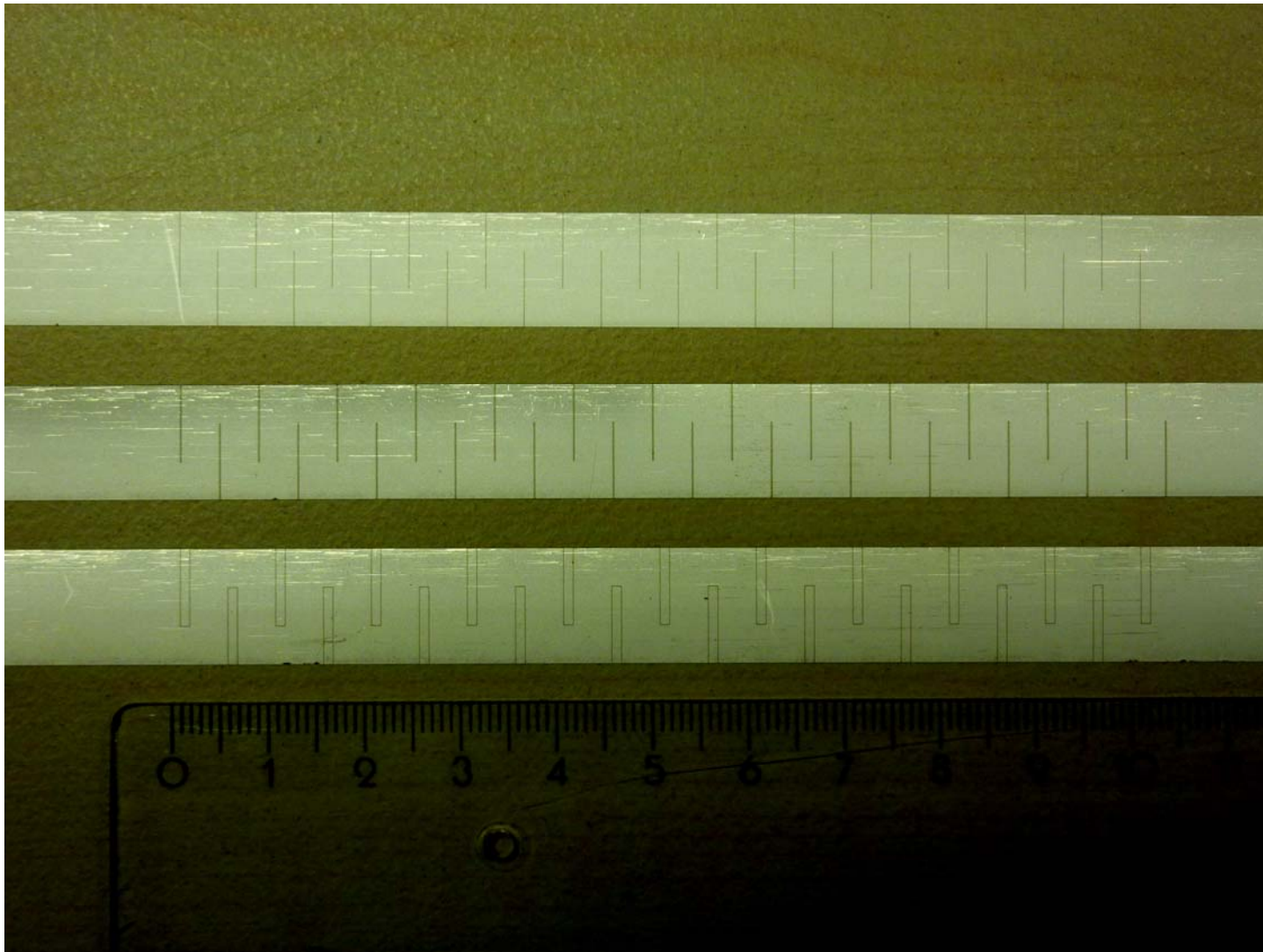
Maximum current 555 A  $\Rightarrow$   $I = 0.92 \text{ kA/mm}^2$

BNG HTS tape undulator @ 4.2K



### Open issues:

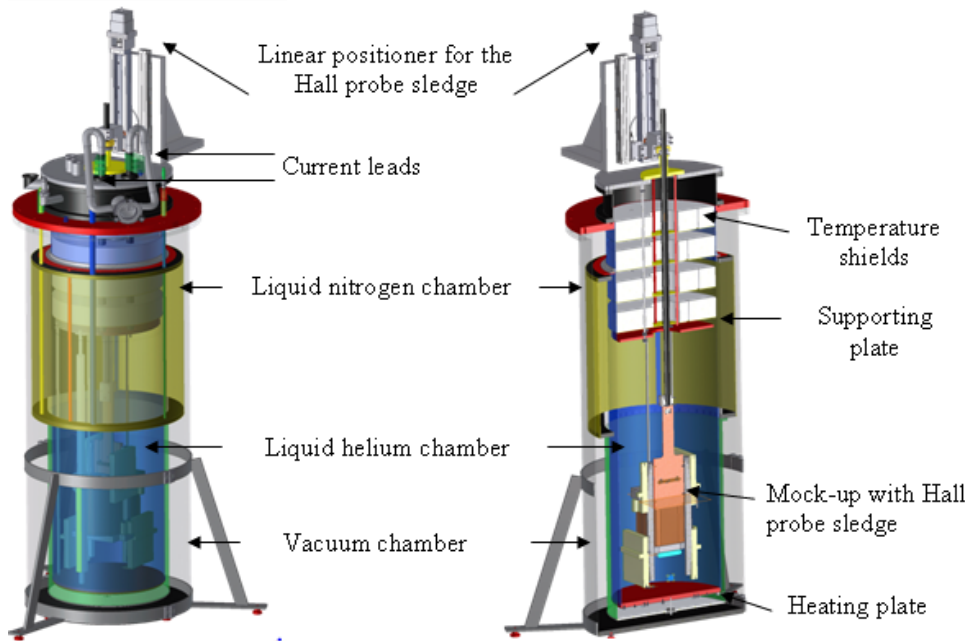
- Joints resistance
- Quench detection and protection
- Test field accuracy
- Radiation damage
- Engineering current density as a function of the magnetic field, geometry, stress



# Tools and instruments for R&D: CASPERI

To test:

- New winding schemes
- New superconducting materials and wires
- New field correction techniques



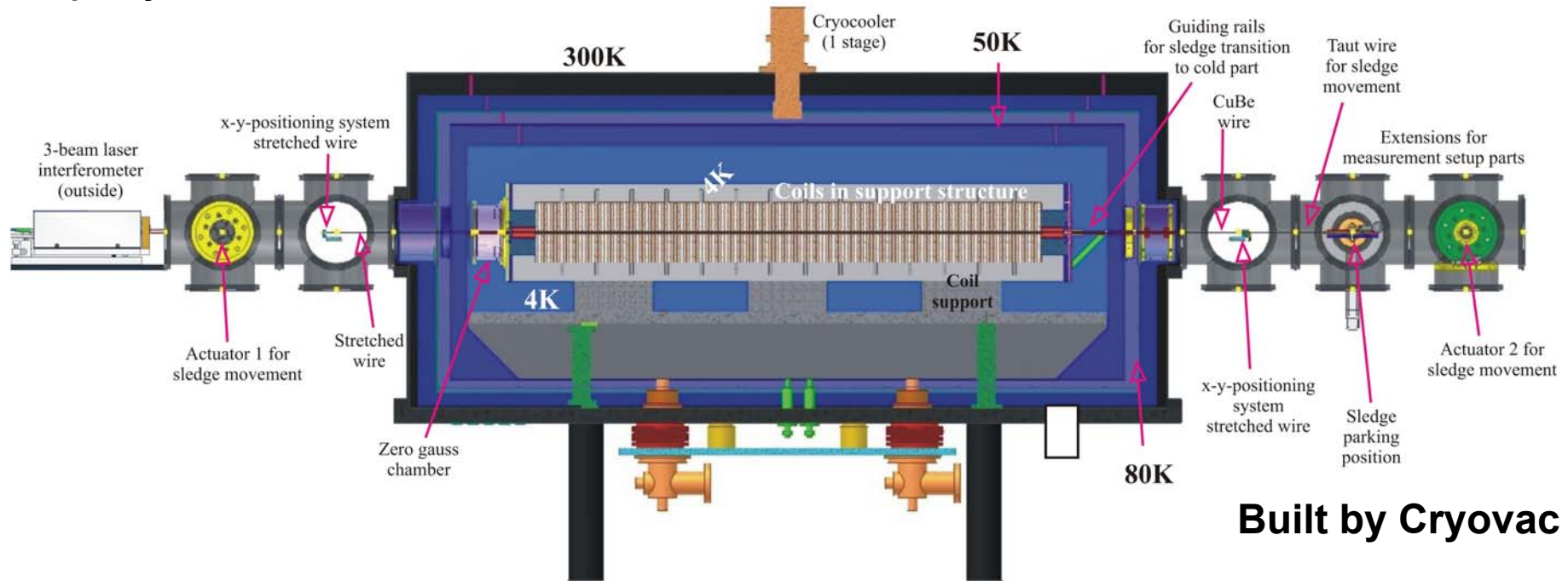
• **Operating vertical test in LHe of mock-up coils** with maximum dimensions 35 cm in length and 30 cm in diameter.

• The magnetic field along the beam axis is measured by Hall probes fixed to a sledge moved by a linear stage with the following precision  $\Delta B < 1\text{mT}$  and  $\Delta z < 3\ \mu\text{m}$ .

E. Mashkina et al., EPAC08

# Tools and instruments for R&D: CASPERII

For quality certification of new sc insertion devices



**Built by Cryovac**

- **Under construction horizontal cryogen free test of long coils** with maximum dimensions 1.5 m in length and 50 cm in diameter.

- Local field measurements with Hall probes. Field integral measurements with stretched wire.

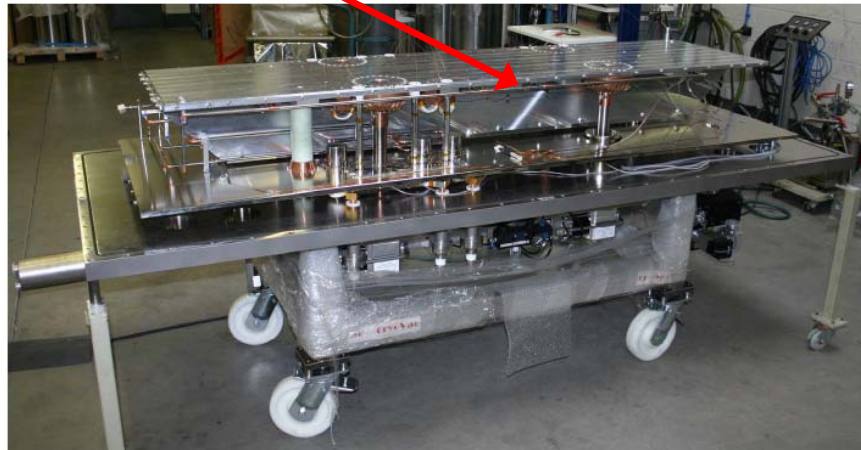
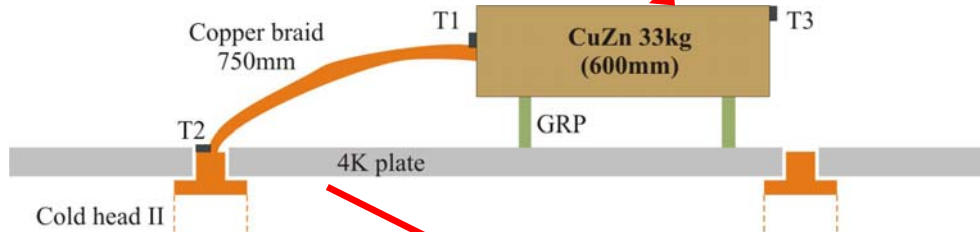
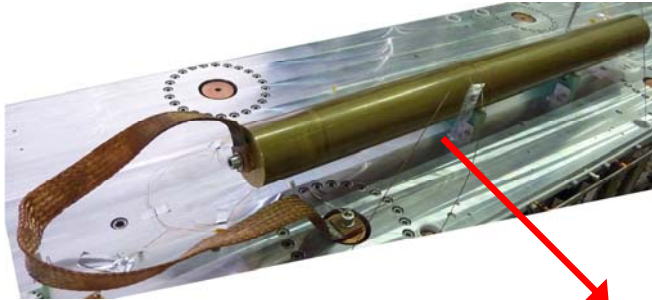
The magnetic field along the beam axis is measured by Hall probes fixed to a sledge moved by a linear stage with the following precision  $\Delta B < 1\text{mT}$  and  $\Delta z = 1 \mu\text{m}$ .

A. Grau et al., IEEE Trans. on Appl. Supercond. 2312-2315 Vol. 21-3 (2011)



# Tools and instruments for R&D: CASPERII

## Factory acceptance test



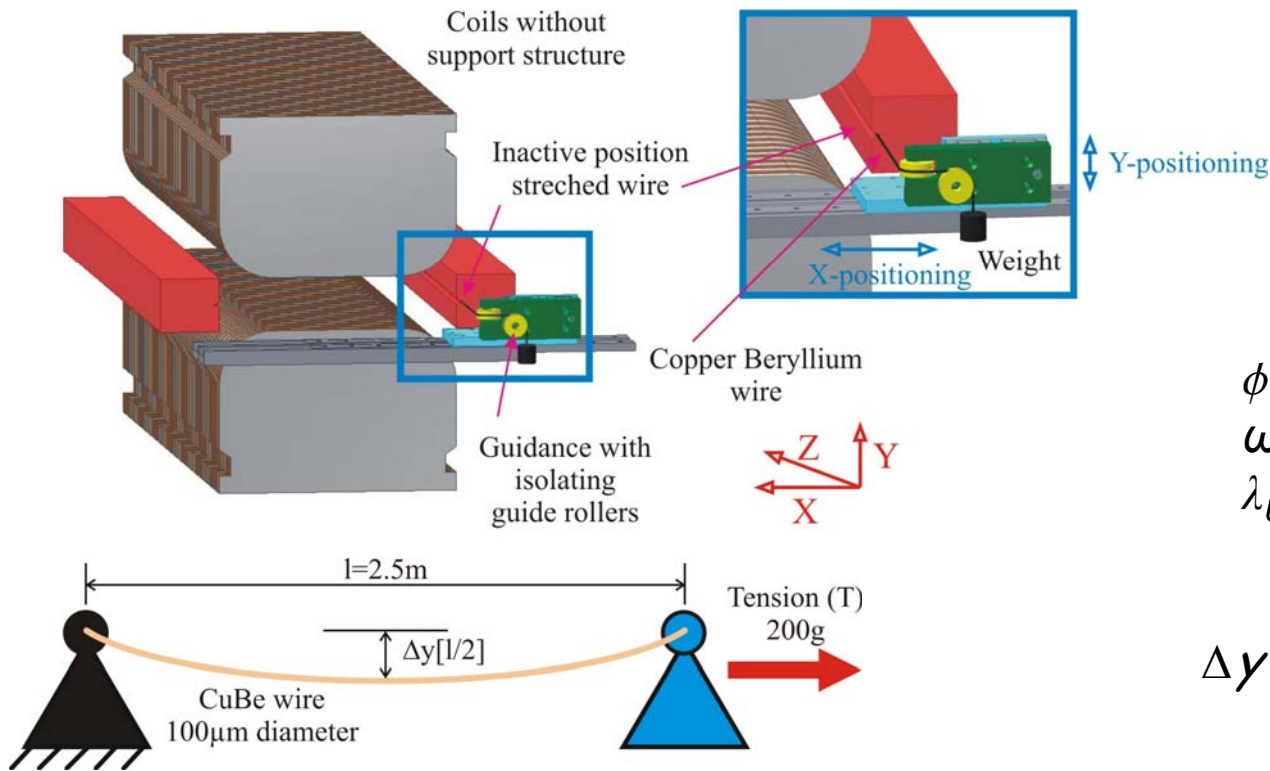
| Component              | Specified value | Reached value |
|------------------------|-----------------|---------------|
| Temperature 80K-plate  | T < 85 K        | Ø 83 K        |
| Temperature 80K-shield | T < 100 K       | Ø 85 K        |
| Temperature 50K-shield | T < 60 K        | Ø 50 K        |
| Temperature 4K-shield  | T < 10 K        | Ø 6.2 K       |
| Temperature 4K-plate   | T < 4.5 K       | Ø 4.5 K       |
| T1                     | targeted < 4 K  | 3.6 K         |
| T2                     | "               | 3.4 K         |
| T3                     | "               | 3.7 K         |



A. Grau et al., MT22, 2011

# Tools and instruments for R&D: CASPERII

## Integral field measurements with stretched wire



$$\begin{aligned} \phi_{CuBe} &= 100 \mu m \\ \omega_{CuBe} &= 0.064 g/m \\ \lambda_U &= 0.015 m \end{aligned}$$

$$\Delta y \left( \frac{l}{2} \right) \cong - \frac{\omega_{CuBe} l^2}{8T}$$

$$\frac{\Delta I_y}{I_y} \approx \frac{1}{2} \left( \frac{2\pi}{\lambda_U} \right)^2 \cosh \left( \frac{2\pi}{\lambda_U} \Delta y \right) (\Delta y)^2 \approx 5 \times 10^{-3}$$

A. Grau et al., IEEE Trans. on Appl. Supercond. 2312-2315 Vol. 21-3 (2011)

# Tools and instruments for R&D: CASPERII

## Local field measurements with Hall probes

**Mechanical requirements to reach measurement accuracy for phase error**

A.Grau et al., IEEE Trans. App. Supercond. 2333- 2336 Vol. 19-3 (2009)

$\Delta\phi = 1^\circ$  ( $\lambda_J=15\text{mm}$ ,  $K=2$ ):

$\Delta x = 400 \mu\text{m}$

$\Delta y = 50 \mu\text{m}$

$\Delta z = 5 \mu\text{m}$

roll = 1 mrad

yaw= 1 mrad

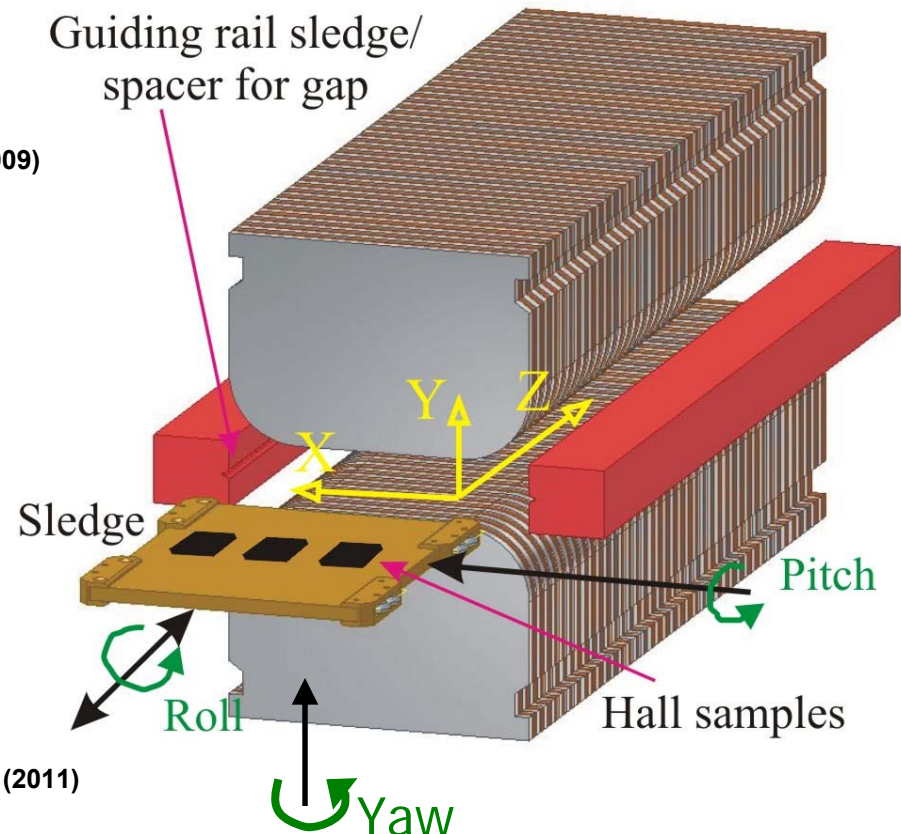
pitch = 30 mrad

**Relative longitudinal position of Hall probes measured with laser interferometer with  $1\mu\text{m}$  accuracy.**

A. Grau et al., IEEE Trans. on Appl. Supercond. 2312-2315 Vol. 21-3 (2011)

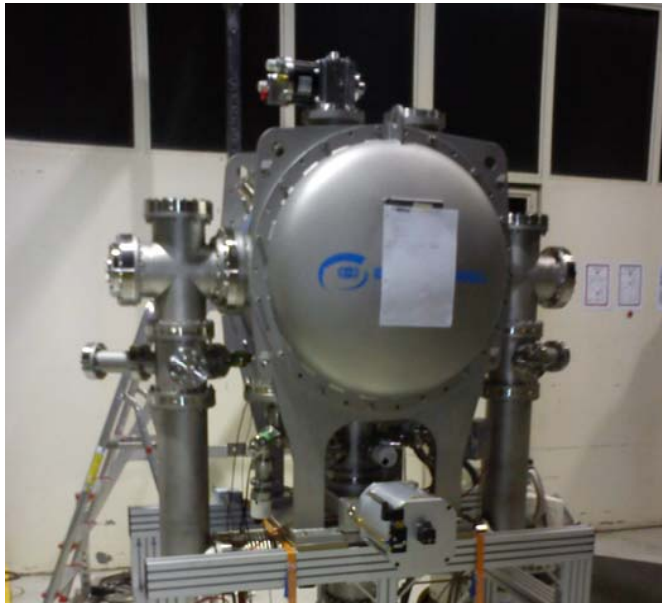
For more details see

<http://immw17.cells.es/presentations/Mon02-IMMW17-AGrau.pdf>





# Tools and instruments for R&D: COLDDIAG



Cold vacuum chamber for diagnostics to **measure the beam heat load** to a cold bore in a storage ring. The beam heat load is needed to specify the cooling power for the cryodesign of superconducting insertion devices.

In collaboration with

**CERN: V. Baglin**

**LNF: R. Cimino, B. Spataro**

**University of Rome ,La sapienza': M. Migliorati**

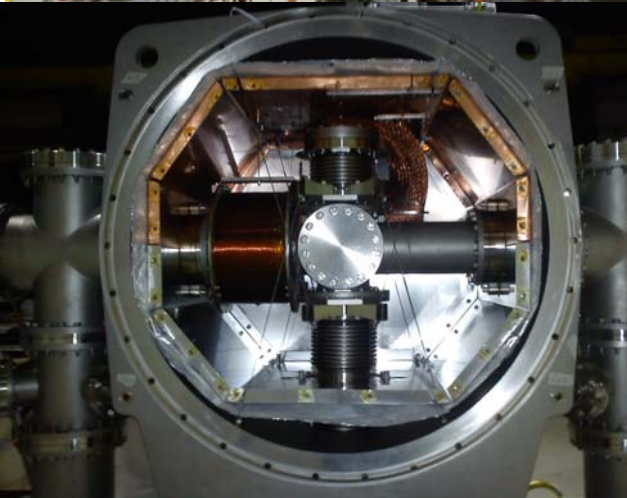
**DIAMOND: R. Bartolini, M. Cox, G. Rehm, J. Schouten, R. Walker**

**MAXLAB : Erik Wallèn**

**STFC/DL/ASTeC: J. Clarke**

**STFC/RAL: T. Bradshaw**

**University of Manchester: I. Shinton**



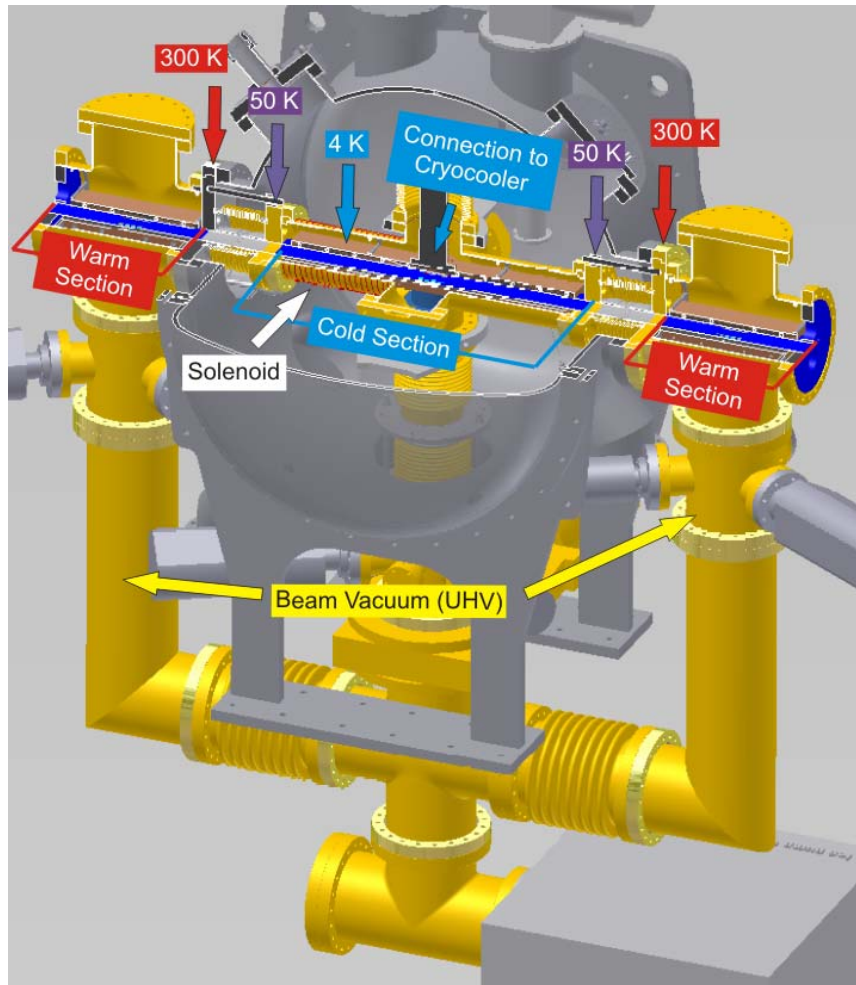
COLDDIAG at DIAMOND: first data expected 2012





# Tools and instruments for R&D: COLDDIAG

## The vacuum chamber



- Cryogen free: cooling with Sumitomo RDK-415D cryocooler (1.5W@4.2K)

- Cold vacuum chamber located between two warm sections to compare beam heat load with and without cryosorbed gas layer

- 3 identically equipped diagnostic ports with room temperature connection to the beam vacuum

- Exchangeable liner to test different materials and geometries

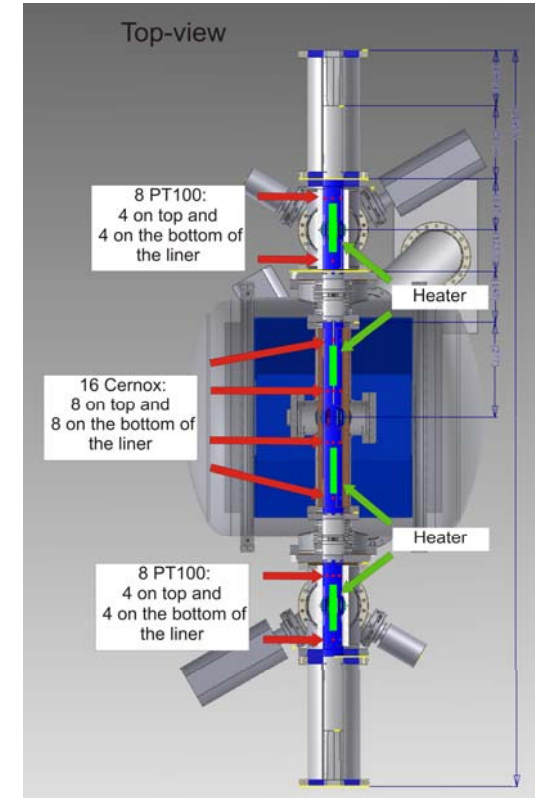
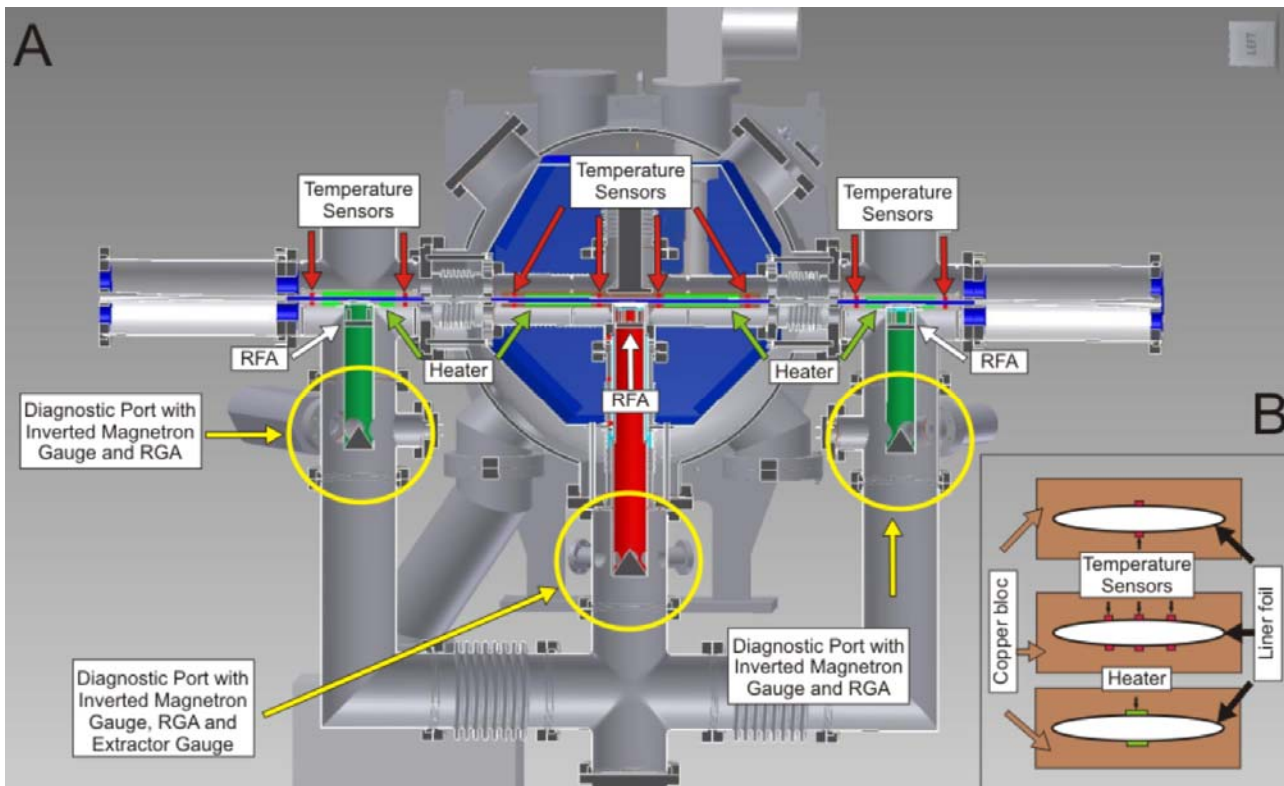
- Copper bar copper plated (50 $\mu$ m)

S.C. et al., IEEE Trans. on Appl. Supercond. 2300-2303 Vol. 21-3 (2011)

# Tools and instruments for R&D: COLDDIAG

## Diagnostics

**Possible Beam Heat Load Sources:** 1) Synchrotron radiation from upstream bending magnet, 2) Resistive wall heating, 3) RF effects, 4) Electron and/ or ion bombardment

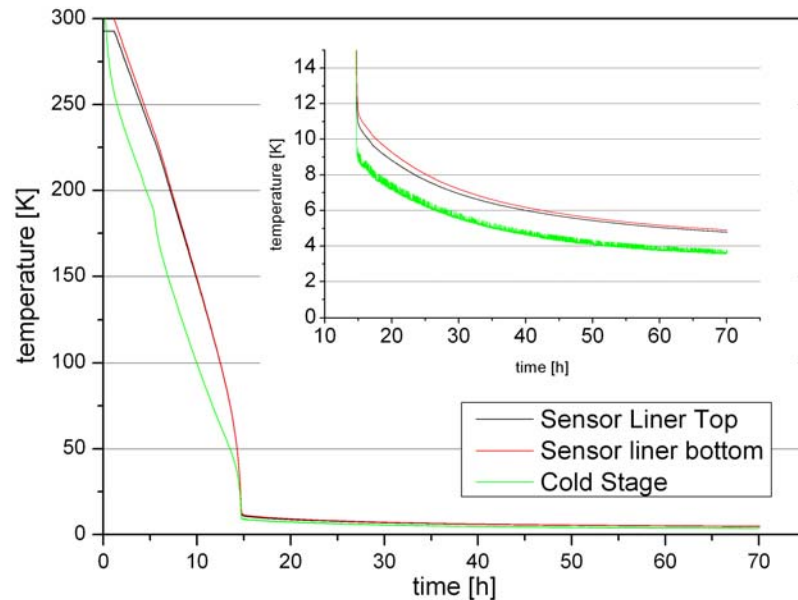


The diagnostics will include measurements of the heat load, the pressure, the gas composition, and the electron flux of the electrons bombarding the wall.

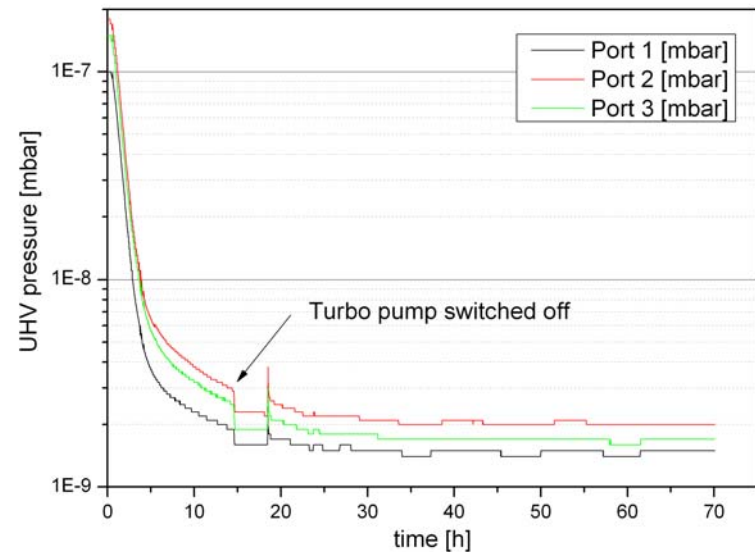
S.C. et al., IEEE Trans. on Appl. Supercond. 2300-2303 Vol. 21-3 (2011)

# Tools and instruments for R&D: COLDDIAG

## Factory acceptance test



- Leakrate UHV:  $<4.3 \times 10^{-10}$  mbar
- Leakrate Insulation Vacuum:  $<8.1 \times 10^{-9}$  mbar
- Lowest Temperature: 4.8 K after 87h
- Pressure at 300 K:  $<2.0 \times 10^{-7}$  mbar
- Pressure at 4.8 K:  $<3.0 \times 10^{-9}$  mbar



S. Gerstl et al., IPAC11, 2011

# Tools and instruments for R&D: COLDDIAG

## Planned measurements

Monitoring the temperature, the electron flux, pressure and gas composition with different:

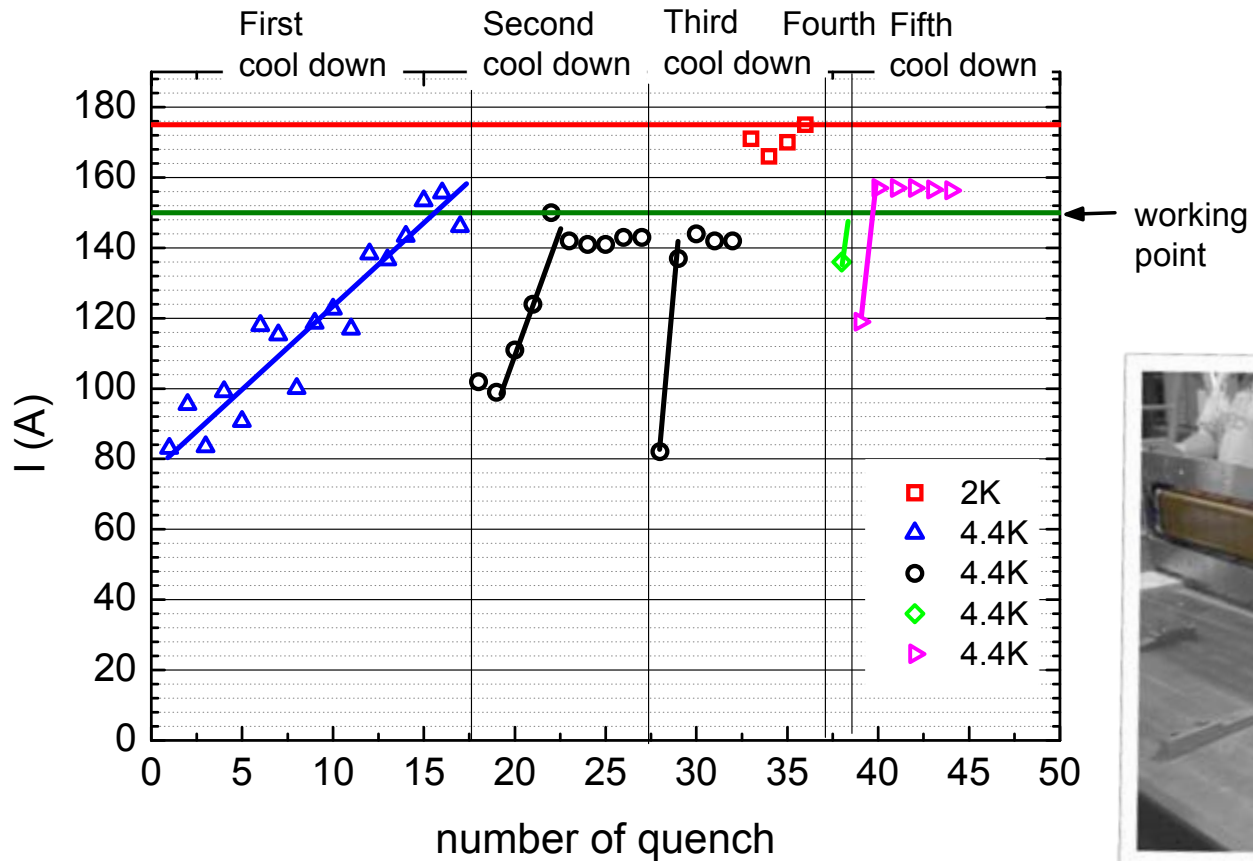
- **average beam current** to compare the beam heat load data with synchrotron radiation and resistive wall heating predictions
- **bunch length** to compare with resistive wall heating predictions
- **filling pattern** in particular the bunch spacing to test the relevance of the electron cloud as heating mechanism
- **beam position** to test the relevance of synchrotron radiation and the gap dependence of the beam heat load
- **injected gases** naturally present in the beam vacuum (H<sub>2</sub>, CO, CO<sub>2</sub>, CH<sub>4</sub>) to understand the influence of the cryosorbed gas layer on the beam heat load



# Backup slides

# SCU15 demonstrator: training

Measured @CERN

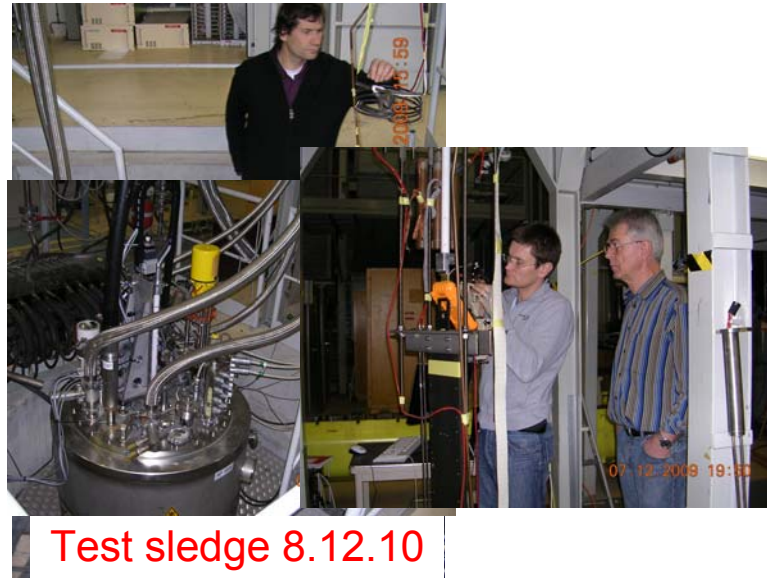
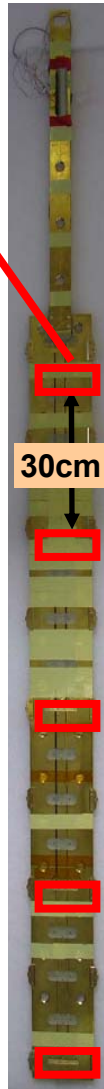
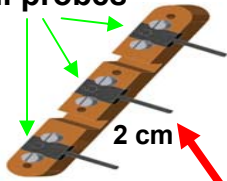


**Next devices thicker wire and for the yoke C10E steel.**

S.C. et al., IEEE Trans. on Appl. Supercond. 1760-1763 Vol. 21-3 (2011)

# Experimental setup

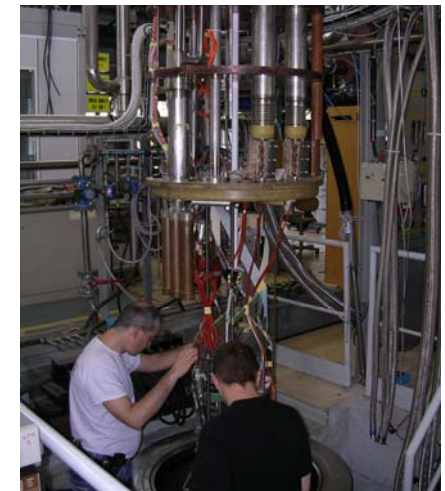
Hall probes



Installation 31.03.10

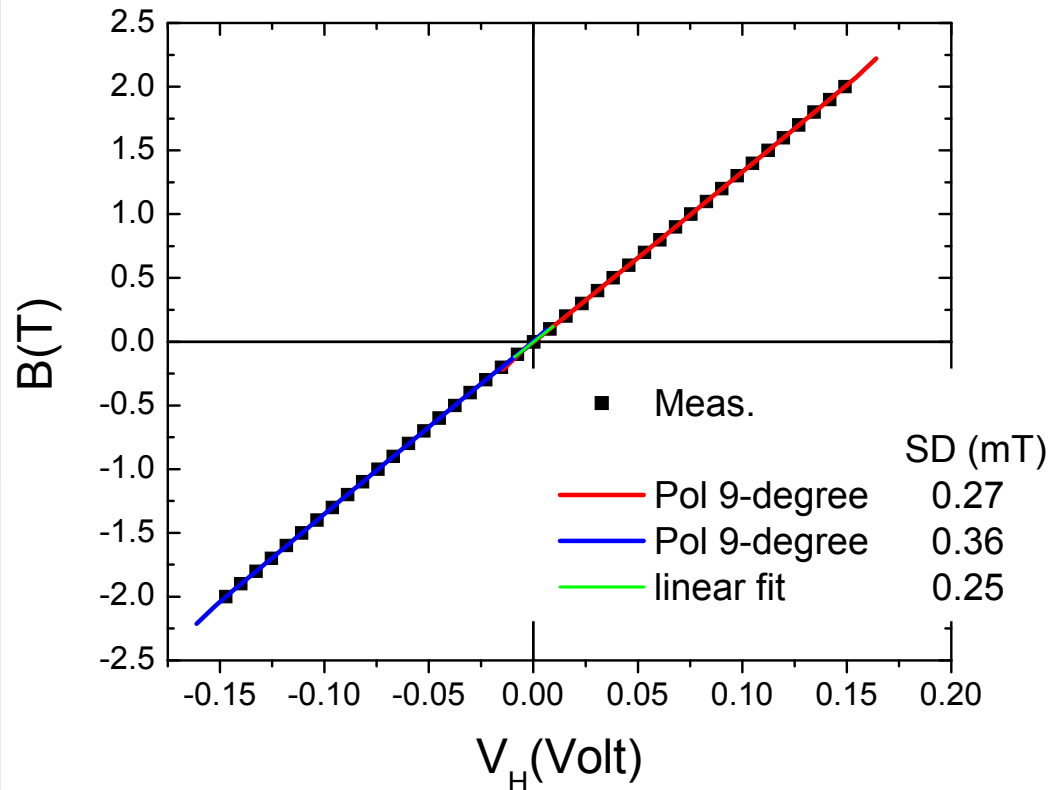


Deinstallation 03.05.10



# Hall probes calibration

Hall probes calibrated at the Institute of Technical Physics (KIT) in a liquid helium bath in a field  $-3\text{T} < B < 3\text{T}$  with homogeneity better than  $10^{-4}$ .



Local phase error induced by calibration of the Hall probes  $\Delta B < 1\text{mT}$ :

$$\Delta\Phi = \frac{K^2}{1+K^2} \frac{\Delta B}{B} 360^\circ < 0.35^\circ$$

$$K = 93.37 \lambda_u B = 1.08$$

$$\lambda_u = 0.015\text{m} \quad B = 0.77\text{T}$$

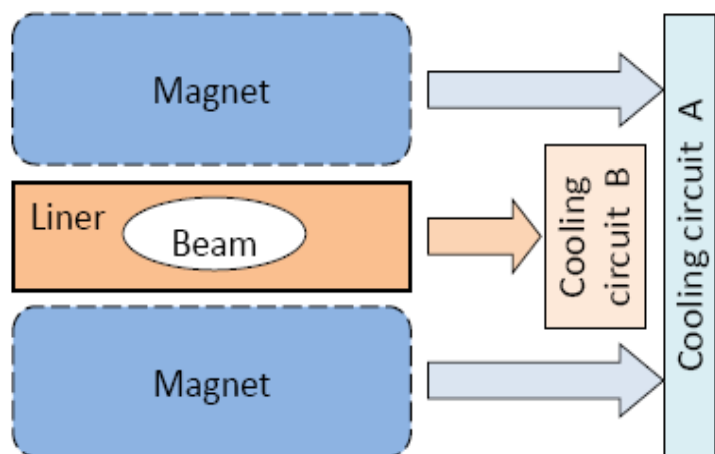
S.C. et al., IEEE Trans. on Appl. Supercond. 1760-1763 Vol. 21-3 (2011)



## Design – Cryogenic circuit

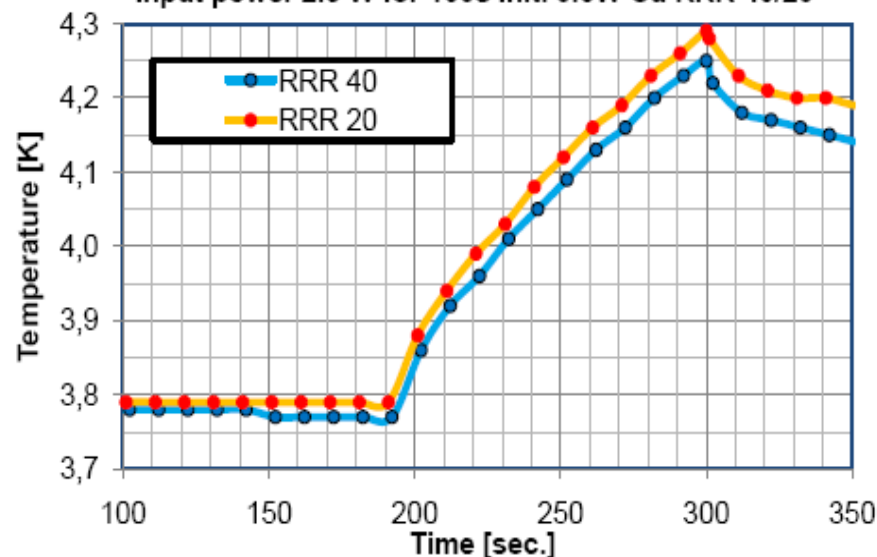
### Main concepts:

- Two separate circuits for magnet and beam liner.
- Two base temperatures: 4K for the magnet and 10K for the beam liner.
- Minimization of gradients between cold head and most distant point in the magnet.

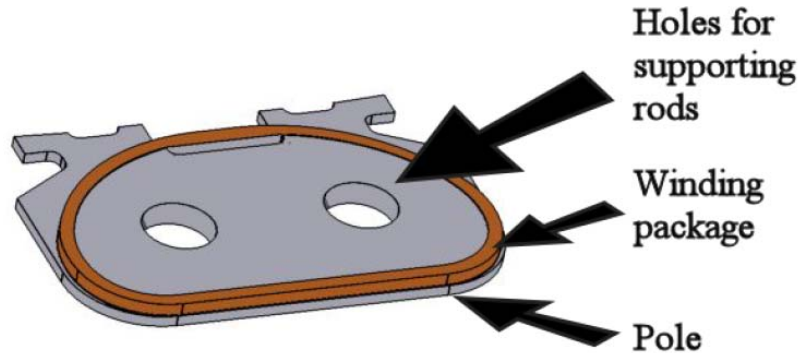


| Watt Loads       |              |             |             |
|------------------|--------------|-------------|-------------|
|                  | Shield       | Circuit B   | Circuit A   |
| Radiation        | 7.93         | 0.05        |             |
| Conduction       | 21.98        | 0.53        | 0.28        |
| Current leads    | 18.80        |             | 0.13        |
| Eddy currents    |              |             | 0.20        |
| Hysteresis       |              |             | 0.14        |
| Coupling SC      |              |             | 1.71        |
| Beam Heat        | 16           | 4.00        |             |
| <b>TOTAL (W)</b> | <b>64.71</b> | <b>4.58</b> | <b>2.46</b> |

Magnet Heating during Ramp -hot spot-  
Input power 2.5 W for 100s Init. 0.5W Cu RRR 40/20

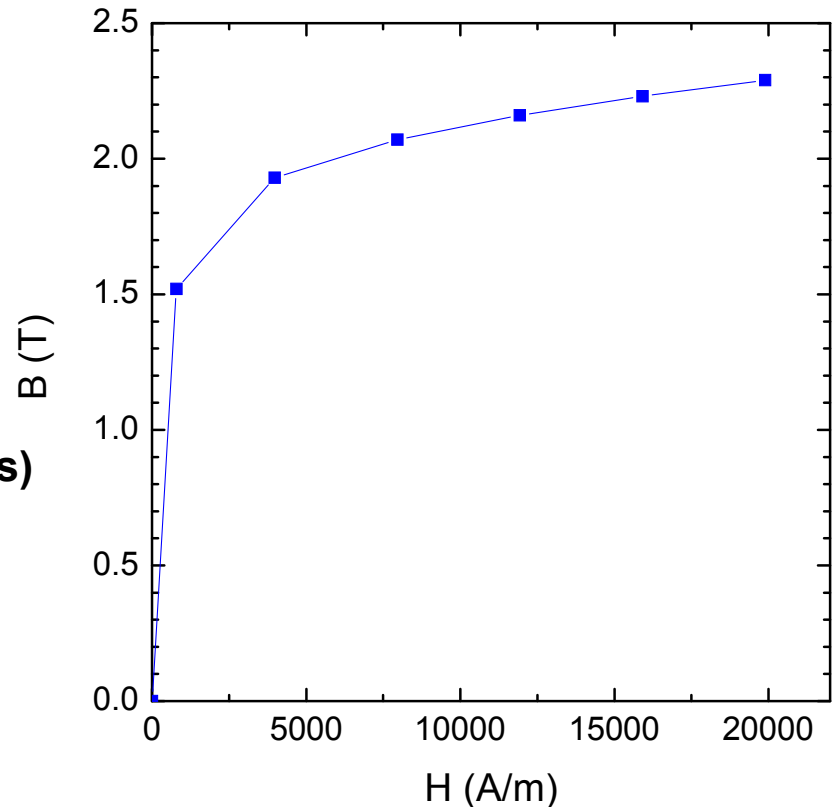


# SCU15 demonstrator



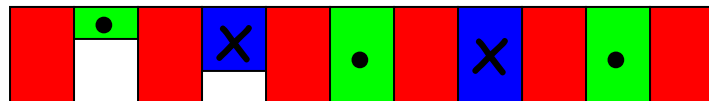
**206 plates of high magnetic field saturation cobalt-iron alloy**

**Magnetization curve of cobalt-iron alloy from constructor @300K**

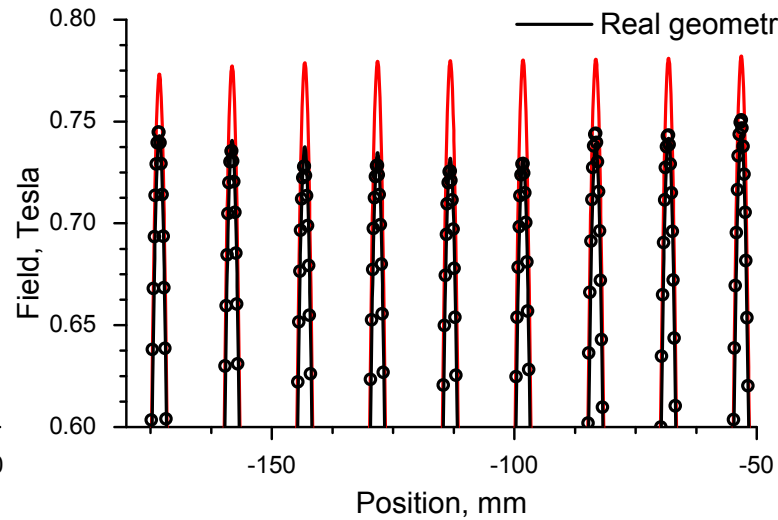
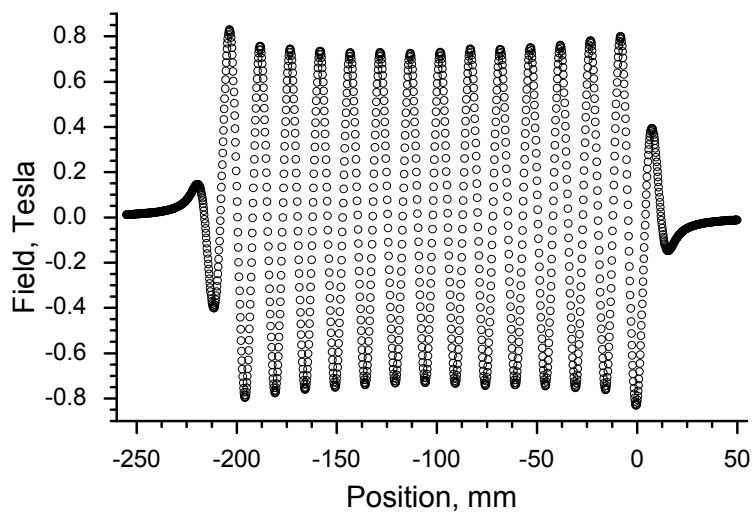


**Cross section NbTi wire:  
0.54mm x 0.34mm (including insulation)**

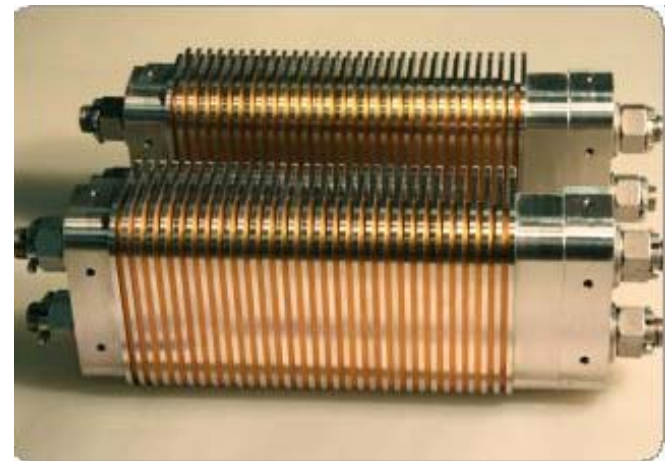
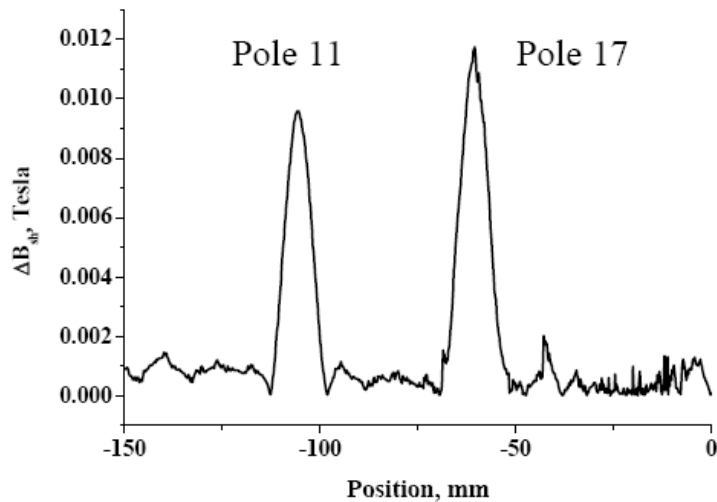
**End fields:  
first winding packages 21 turns (3 layers)  
second winding packages 63 turns (9 layers)**



# SCU15 prototype



## Active shimming using racetrackcoils



S. C. et al., SRI 2009, AIP-Conf. Proc. 33-36 Vol. 1234 (2010).

# Experience at ANKA: SCU14 demonstrator

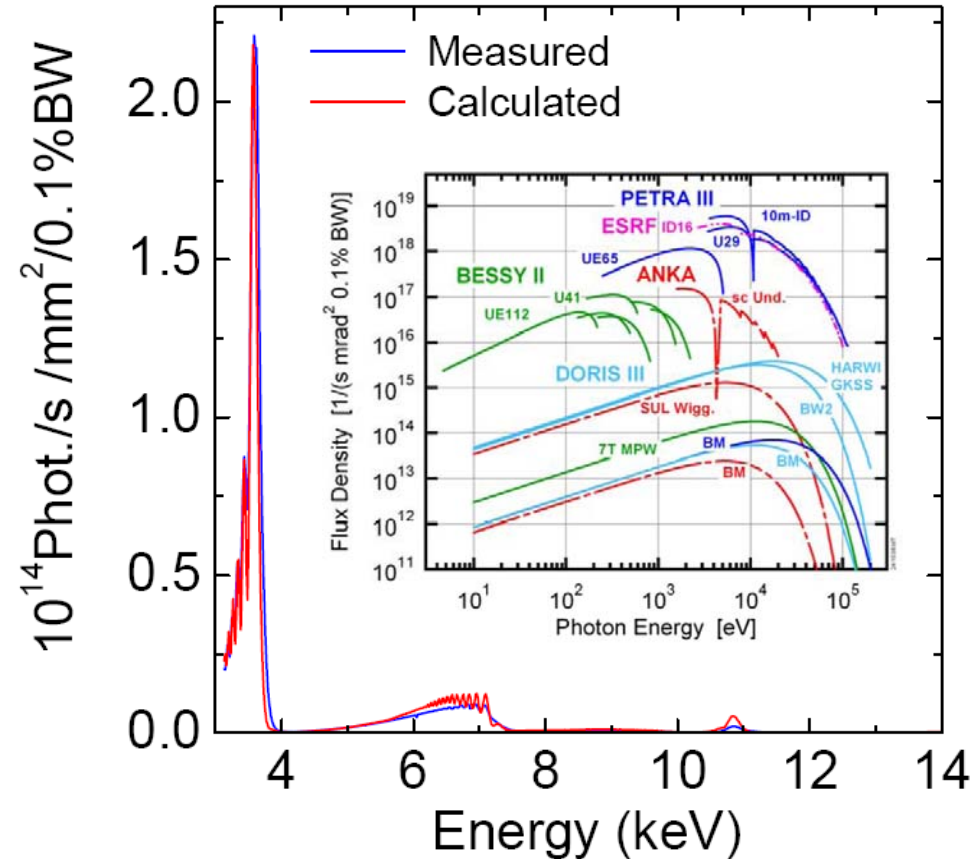
Proof of principle of scu technology first time worldwide demonstrated at ANKA (2005) developed in collaboration with ACCEL.

- Period length: 14 mm
- Length: 100 periods
- NbTi - coils



■ Outcome used:

- to measure beam heat load to a cold vacuum chamber at ANKA
- to improve the design of next generation sc undulators

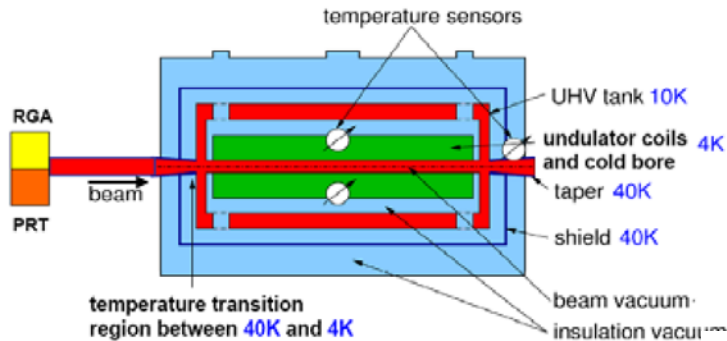


R. Rossmanith et al., SRI 2006, AIP-Conf. Proc. 301-304 Vol. 879 (2007).

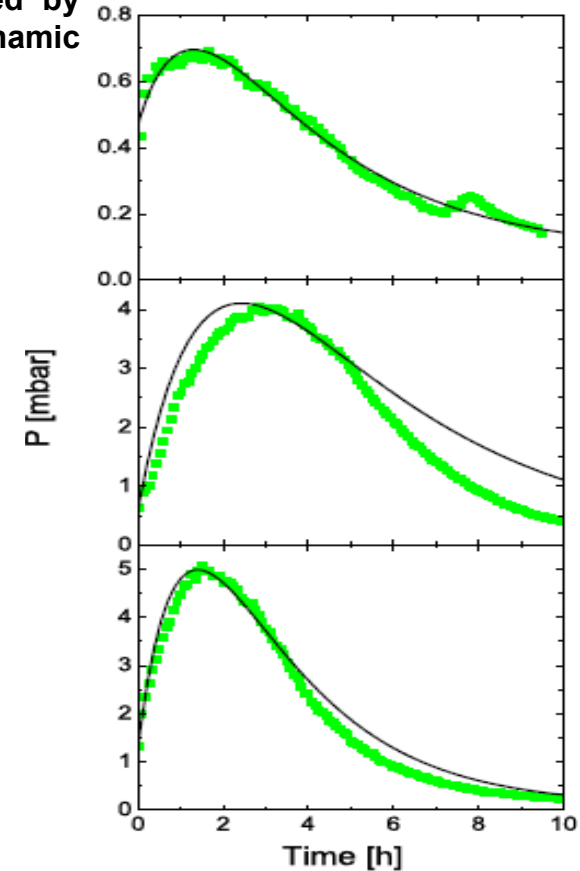
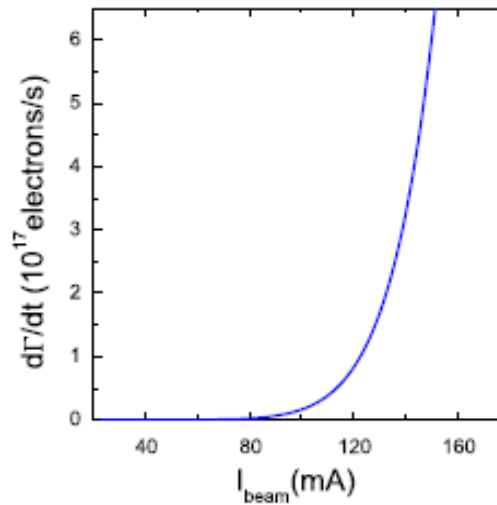
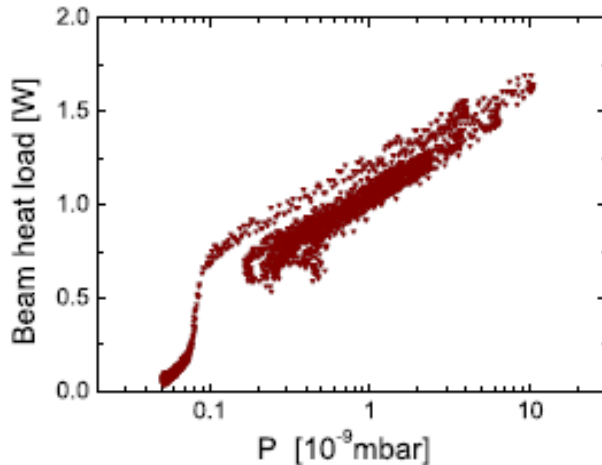


# Experience at ANKA: SCU14 demonstrator

Performance limited by too high beam heat load: beam heat load observed cannot be explained by synchrotron radiation from upstream bending and resistive wall heating. S. C. et al., PRSTAB2007



Pressure rise can be explained by including in eq. of gas dynamic balance electron multipacting. S. C. et al., PRSTAB2010



Possible beam heat load source: electron bombardment of the wall, beam dynamics under study